

### High Efficiency 1MHz, 33V Output, Boost Converter

### **General Description**

The SY26533 is a high efficiency, current-mode control, asynchronous Boost converter with an integrated  $400m\Omega$   $R_{DS(ON)}$  N-channel MOSFET. The fixed 1MHz switching frequency and internal compensation reduce external component count and save PCB space. The built-in internal soft start circuitry minimizes the inrush current at start-up.

When disabled SY26533 consumes only 5  $\mu\text{A}$  of quiescent current to save power.

The device offers cycle-by-cycle current and thermal protections to ensure reliable operation.

#### **Features**

- Wide Input Range: 3-30V
- Output Voltage Range: VIN to 33Vout, MAX
- 1MHz Switching Frequency
- Minimum ON Time: 100ns typicalMinimum OFF Time: 100ns typical
- Low R<sub>DS(ON)</sub>: 400mΩ
- RoHS Compliant and Halogen Free
   Accurate Reference: 1.24V<sub>REF</sub>
- Compact Package: SOT23-6

## **Applications**

- Digital Cameras
- PDA, PMP, MP3
- LED/ Backlight Drivers

### **Typical Application**

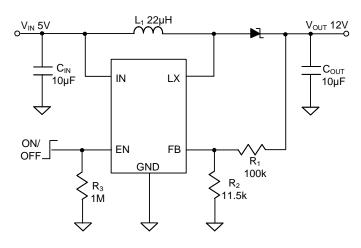


Figure 1. Schematic Diagram

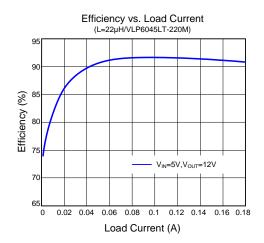


Figure 2. Efficiency vs. Load Current

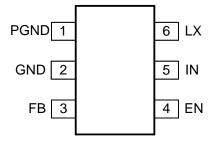


## **Ordering Information**

Ordering Part Number	Package Type	Top Mark
SY26533ABC	SOT23-6 RoHS Compliant and Halogen Free	Y8 <i>xyz</i>

x=year code, y=week code, z= lot number code

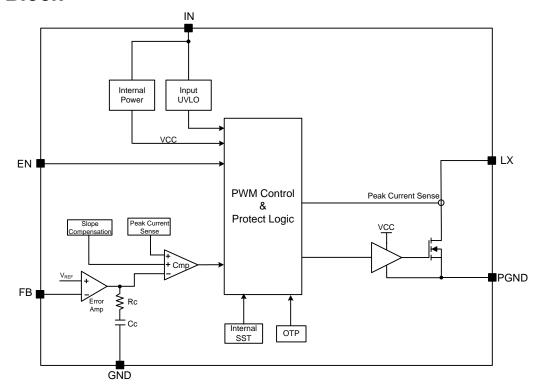
## Pinout (top view)



## **Pin Description**

Pin Name	Pin Number	Pin Description		
PGND	1	Power ground pin.		
GND	2	Signal ground pin.		
FB 3 Feedback pin. Connect a resistor R <sub>1</sub> between V <sub>OUT</sub> and FB, and a resistor R <sub>2</sub> between and GND to program the output voltage: V <sub>OUT</sub> =1.24V×(R <sub>1</sub> /R <sub>2</sub> +1).				
EN	4	Enable control. Drive high to turn on the device. Don't leave it floating.		
IN	5	Input pin. Decouple this pin to the GND pin with a 10µF ceramic capacitor.		
LX	6	Inductor node. Connect an inductor between the IN pin and the LX pin.		

## **Function Block**



Figue3. Block Diagram



### **Absolute Maximum Ratings**

Parameter (Note 1)	Min	Max	Unit
LX	-0.3	36	
IN, EN	-0.3	33	V
FB	-0.3	4	V
LX, 50ns Duration	IN+3	GND-4	
Lead Temperature (Soldering, 10 sec.)		260	
Junction Temperature, Operating	-40	150	°C
Storage Temperature	-65	150	

#### **Thermal Information**

Parameter (Note 2)	Тур	Unit
θ <sub>JA</sub> Junction-to-ambient Thermal Resistance	161	°C/W
θ <sub>JC</sub> Junction-to-case Thermal Resistance	130	C/VV
P <sub>D</sub> Power Dissipation T <sub>A</sub> =25°C	0.6	W

## **Recommended Operating Conditions**

Parameter (Note 3)	Min	Max	Unit
IN	3	30	V
Junction Temperature, Operating	-40	125	ک
Ambient Temperature	-40	85	C

### **Electrical Characteristics**

(V<sub>IN</sub> = 5V, V<sub>OUT</sub>=12V, I<sub>OUT</sub>=100mA, T<sub>J</sub>= -40°C to +125°C. Typical values are at T<sub>J</sub>=25°C, unless otherwise specified. The values are guaranteed by test, design or statistical correlation.)

Parameter	Symbol	Test Conditions	Min	Тур	Max	Unit
Input Voltage Range	Vin		3		30	V
IN UVLO Rising Threshold	Vin, uvlo		1.3		2.2	V
Quiescent Current	ΙQ	V <sub>FB</sub> =1.3V		100	150	μΑ
Shutdown Current	I <sub>SHDN</sub>	EN=0		5	20	μΑ
Low Side Main FET Ron	R <sub>DS(ON)</sub>			400	600	mΩ
Main FET Current Limit	I <sub>LIM1</sub>	55% Duty cycle	450	750	925	mΑ
Main FET Leakage Current	I <sub>LK</sub>	EN=0			1	μΑ
Switching Frequency	fsw		0.8	1	1.32	MHz
Feedback Reference Voltage	V <sub>REF</sub>		1.21	1.24	1.265	V
EN Rising Threshold	VENH		1.5			V
EN Falling Threshold	VENL				0.4	V
EN Leakage Current	I <sub>EN</sub>	EN=5V	-1		1	μΑ
Max Duty Cycle	D <sub>MAX</sub>		85	90		%
Min ON Time	ton, min			100	150	ns
Min OFF Time	toff, MIN			10%	15%	Ts
Thermal Shutdown Temperature	T <sub>SD</sub>			150		°C
Thermal Shutdown Hysteresis	T <sub>HYS</sub>			10		°C

**Note 1**: Stresses beyond "Absolute Maximum Ratings" may cause permanent damage to the device. These are for stress ratings. Functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.





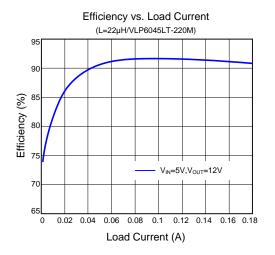
**Note 2**:  $\theta_{\text{JA}}$  is measured in the natural convection at  $T_{\text{A}}$  = 25°C on a low effective single layer thermal conductivity test board of JEDEC 51-3 thermal measurement standard. Test condition: Device mounted on 2" x 2" FR-4 substrate PCB, 2oz copper, with minimum recommended pad on top layer and thermal vias to bottom layer ground plane.

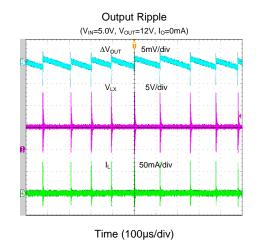
**Note 3:** The device is not guaranteed to function outside its operating conditions.

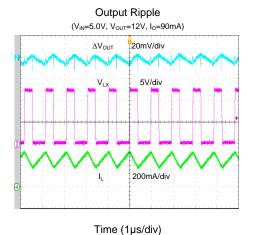


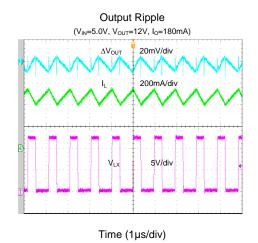
# **Typical Performance Characteristics (Boost)**

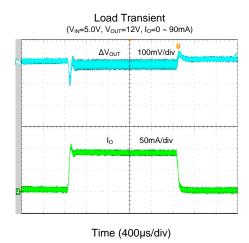
 $(T_A= 25^{\circ}C, V_{IN}=5V, V_{OUT}= 12V, L= 22\mu H, C_{OUT}= 10\mu F, unless otherwise specified)$ 

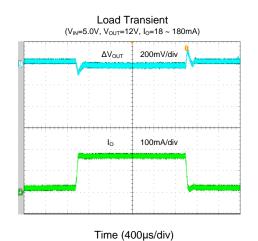




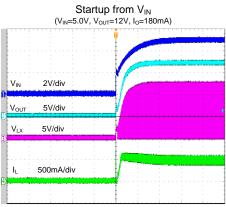


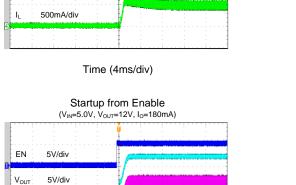










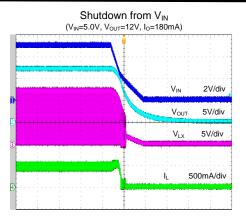


Time (2ms/div)

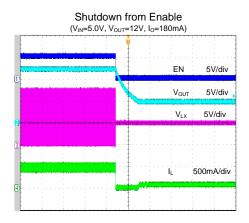
 $V_{\mathsf{LX}}$ 

5V/div

500mA/div



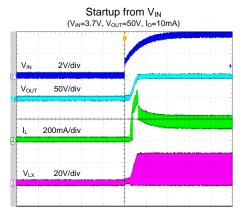
Time (2ms/div)



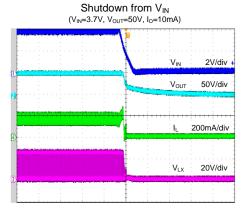
Time (800µs/div)



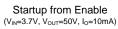
# **Typical Performance Characteristics (Charge pump)**

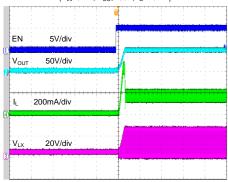


Time (4ms/div)

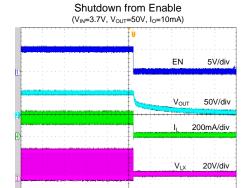


Time (4ms/div)

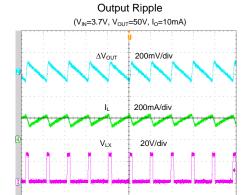




Time (2ms/div)



Time (2ms/div)



Time (1µs/div)



## **Applications Information**

The SY26533 regulates the output using a peak current mode control loop. The device operates at a fixed frequency of around 1MHz. Each switching cycle starts by the MOSFET being turned on. As a result, the current through the inductor ramps up. The MOSFET is turned off when the current reaches the threshold level set by the error amplifier output. When the power MOSFET turns off, the external Schottky diode starts conducting. The operation repeats every switching cycle. An internal slope compensation is used to avoid subharmonic oscillation at duty cycles higher than 50%.

The following paragraphs provide information on selecting the components required when designing with SY26533, in order to meet the target specifications.

#### Feedback Resistor Dividers R1 and R2:

Choose R<sub>1</sub> and R<sub>2</sub> to program the proper output voltage. To minimize the power consumption under light loads, it is desirable to choose large resistance values for both R<sub>1</sub> and  $R_2$ . A value of between  $10k\Omega$  and  $100k\Omega$  is recommended for both resistors. If R<sub>1</sub>=is chosen, then R<sub>2</sub> can be calculated to be:

$$R_2 = (R_1 \times 1.24 \text{V})/(V_{\text{OUT}} - 1.24 \text{V})$$
 $R_2 = (R_1 \times 1.24 \text{V})/(V_{\text{OUT}} - 1.24 \text{V})$ 
 $R_2 = (R_1 \times 1.24 \text{V})/(V_{\text{OUT}} - 1.24 \text{V})$ 

#### Input Capacitor Cin:

When selecting an input capacitor ensure that its voltage rating is at least 20% greater than the maximum voltage of the input supply. X5R or X7R dielectric types are the most often selected due to their small size, low cost, surge current capability and high RMS current rating over wide temperature and voltage ranges.

In situations where the input rail is supplied through long wires it is recommended adding some bulk capacitance like electrolytic, tantalum or polymer type capacitors to reduce the overshoot and ringing caused by the added parasitic inductance.

Consider the RMS current rating of the input capacitor, paralleling additional capacitors if required to reduce the input voltage ripple.

A single 10 µF X5R capacitor is recommended for most applications.

#### **Output Capacitor Cout:**

The output capacitor is selected to handle the output ripple requirements. Both steady state ripple and transient requirements must be taken into consideration when selecting this capacitor. For the best performance, it is recommended to use a X5R or better grade ceramic capacitor with 50V rating and more than 10µF capacitance. Additional information on how to calculate the output capacitance required for meeting a target maximum voltage ripple is presented below:

When the main MOSFET is in the ON state, the switching current flowing to the load is filtered by the output capacitor. The voltage ripple is proportional with the load current. The minimum capacitance required for a specified output voltage ripple can be calculated using the following formula:

$$C_{OUT} = I_{LOAD} \times \frac{D}{(\Delta V_{OUT} \times fsw)}$$

Where ILOAD is the maximum load current, D is the dutycycle and  $\Delta V_{OUT}$  is the maximum acceptable voltage ripple. The output voltage ripple contribution from the output capacitor(s) ESR can be calculated as:

$$\Delta V_{ESR} = I_{LOAD} \times R_{ESR}$$

 $\Delta {\rm V}_{\rm ESR} = {\rm I}_{\rm LOAD} \times {\rm R}_{\rm ESR}$  Where Resr represents the equivalent series resistance of the output capacitors.

The total output ripple is the sum of the ripple caused by the capacitance and the ripple caused by the ESR of the capacitor.

#### **Boost Inductor L:**

There are several considerations in choosing this inductor.

1) Choose the inductance to provide the desired ripple current. It is suggested to choose the ripple current to be about 40% of the maximum average input current. The inductance is calculated as:

$$L = \left(\frac{V_{\rm IN}}{V_{\rm OUT}}\right)^2 \frac{(V_{\rm OUT} - V_{\rm IN})}{f_{sw} \times I_{\rm OUT\_MAX} \times 40\%}$$

Where  $f_{SW}$  is the switching frequency and  $I_{OUT\ MAX}$  is the maximum load current.

The SY26533 is tolerant to different ripple current amplitudes. Consequently, the final choice of the inductance can be slightly different than the calculated value without significantly impacting the performance.

The saturation current rating of the inductor must be selected to be greater than the peak inductor current under full load conditions.



$$I_{\text{SAT,MIN}} > \left(\frac{V_{\text{OUT}}}{V_{\text{IN}} \times \eta}\right) \times I_{\text{OUT\_MAX}} + \frac{V_{\text{IN}}(V_{\text{OUT}} - V_{\text{IN}})}{2 \times f_{\text{SW}} \times L \times V_{\text{OUT}}}$$

3) The DCR of the inductor and the core loss at the switching frequency must be low enough to achieve the desired efficiency requirement. It is desirable to choose an inductor with DCR<50m $\Omega$  to achieve a good overall efficiency.

#### **Enable Operation**

Pulling the EN pin low (<0.4V) will shut down the device. During the shutdown mode, the SY26533 current is reduced to lower than 5 $\mu$ A. Driving the EN pin high (>1.5V) enables normal operation.

#### **Soft-start (EN Control)**

The SY26533 has a built-in soft-start to control the rise rate of the output voltage and limit the inrush current during the start-up.

#### **Diode Selection**

Using a Schottky diode is recommended for achieving high efficiency, because of its low forward voltage drop and fast reverse recovery.

The Schottky diode reverse breakdown voltage should be higher than the maximum output voltage in the application.

The peak current through the Schottky diode is equal to the minimum saturation current of inductor estimated as:

$$I_{\text{PEAK\_DIODE}} \left( \frac{V_{\text{OUT}}}{V_{\text{IN}} \times \eta} \right) \times I_{\text{OUT\_MAX}} + \frac{\Delta I_L}{2}$$

 $\Delta \mathit{IL}$  is the inductor current ripple and can be calculated using the equation:

$$\Delta I_L = \frac{V_{IN} \times D}{f_{SW} \times L}$$

Where D is the duty-cycle, and can be calculated assuming that the device operates in continuous conduction mode (CCM) and at maximum load:

$$D = \frac{V_{\text{OUT}} - V_{\text{IN\_MIN}}}{V_{\text{OUT}}}$$

As an example, for a maximum load current of 50 mA, Vinmin = 4.5V, Vout = 30V, L = 22  $\mu$ H and  $\eta$  = 0.8 the following values can be calculated to obtain the maximum current through the Schottky diode: D = 0.85

$$\Delta IL = 0.174 A$$

 $I_{PEAK\ DIODE} = 0.504A$ 

A diode that can handle 1A of continuous current is recommended for most applications.

#### **Light Load Operation**

The SY26533 operates in burst mode during light load conditions to maintain high-efficiency. DCM operation is automatically initiated when the inductor current falls to zero. As the load decreases further the resulting switching frequency will also decrease in order to keep the output close to the target value.

#### **Overcurrent Protection**

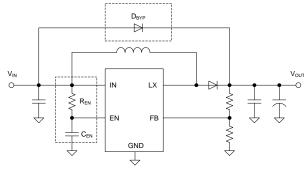
The SY26533 provides cycle by cycle overcurrent protection and turns off the power MOSFET once the inductor current reaches the overcurrent limit threshold. The limit status resets itself at the beginning of the next switching cycle. During the overcurrent protection, the output voltage drops as a function of the load on the output.

#### Thermal protection

The SY26533 includes over temperature protection circuitry to prevent overheating due to excessive power dissipation. This will shut down the device when the junction temperature exceeds 150°C. Once the junction temperature cools down by approximately 10°C, the device will resume normal operation after a complete soft-start cycle. For continuous operation, provide adequate cooling so that the junction temperature does not exceed the thermal protection threshold.

#### **Applications with Large Bulk Capacitance**

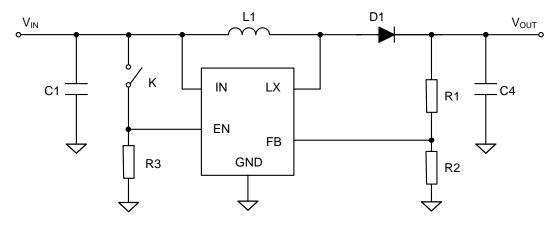
In applications with large bulk capacitance present on the output, a very high inrush current could flow through the inductor during power on. In order to limit the current flowing into the device and prevent damage, a Schottky diode connected from power input to the output, or a RC delay circuit added on the EN pin are recommended as shown below:





### **Typical Design**

### **Typical Schematic**



### **Design Specifications**

Input Voltage (V)	Output Voltage (V)	Output Current Limit (A)
5-12	12	0.18

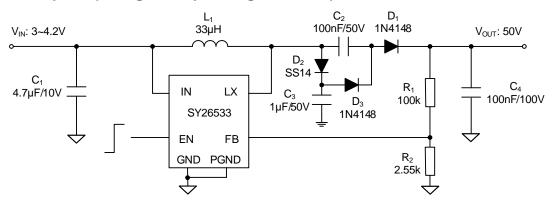
#### **BOM List**

Designator	Description	Part Number	Manufacturer
C <sub>1</sub> , C <sub>4</sub>	10μF/25V, 1206	C3216X7R1E106K	TDK
L <sub>1</sub>	22µH	VLP6045-220M	
D <sub>1</sub>	3A/40V, Schottky	SS34	
R <sub>1</sub>	105kΩ, 1%, 0603		
R <sub>2</sub>	12kΩ, 1%, 0603		
R3	1ΜΩ, 1%, 0603		

### **Recommend Table for Typical Applications**

V <sub>OUT</sub> (V)	R <sub>H</sub> (kΩ)	$R_L(k\Omega)$	L(µH)	C <sub>OUT</sub>
12	105	12	22	10μF/25V/X7R,1206

### **Application Example 2 (Charge Pump Voltage Doubler)**





#### **Layout Design**

The guidelines for the SY26533 regulator layout are presented below:

- 1) Place the following components close to the IC:  $C_{IN}$ , L,  $R_1$  and  $R_2$ .
- 2) It is desirable to maximize the PCB copper area connecting to ground pin to achieve the best thermal transfer of the head and reduce switching noise. If the board space allows it, a ground plane or a large copper pour is highly desirable.
- 3)  $C_{\text{IN}}$  must be close to the IN pin and ground pin. The loop area formed by  $C_{\text{IN}}$  and ground pin must be minimized.

- 4) The PCB copper area associated with the LX pin must be minimized.
- 5) The components  $R_1$ ,  $R_2$  and the trace connecting to the FB pin must NOT be adjacent to the LX net on the PCB layout to avoid crosstalk.
- 6) If the system chip interfacing with the EN pin has a high impedance state during shutdown, and the IN pin is connected directly to a power source such as a Li-Ion battery, it is desirable to add a pull-down  $1M\Omega$  resistor between the EN and ground pins to prevent the noise from falsely turning on the regulator during shutdown.

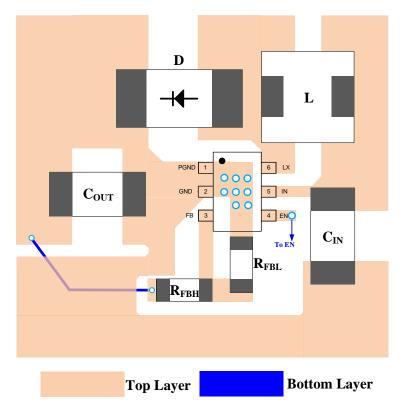


Fig.4 Boost Application



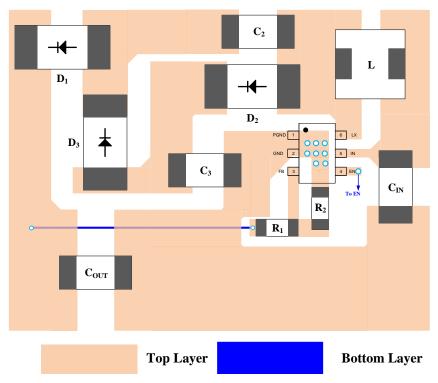
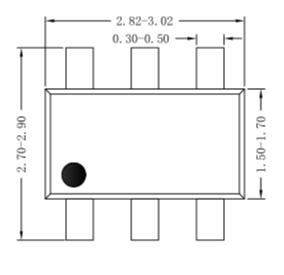


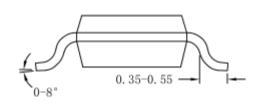
Fig.5 Charge Pump Application



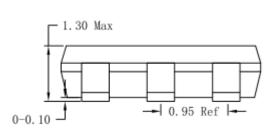
# SOT23-6 Package Outline & PCB Layout Design



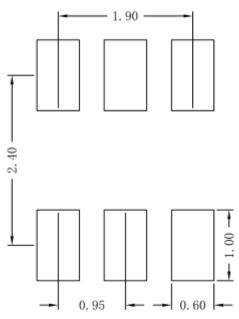
**Top View** 



**Side View** 



**Side View** 



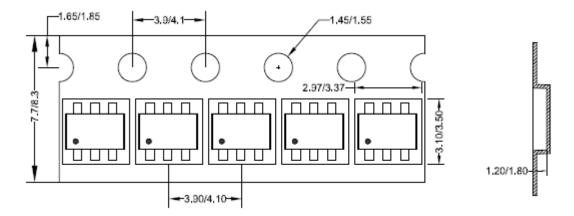
**Recommended Pad Layout** 

Notes: All dimension in millimeter and exclude mold flash & metal burr.



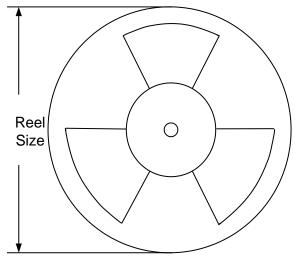
# **Taping & Reel Specification**

## 1. Taping orientation for packages (SOT23-6)



Feeding direction -----

## 2. Carrier Tape & Reel specification for packages



Package type	Tape width (mm)	Pocket pitch(mm)	Reel size (Inch)	Trailer length (mm)	Leader length (mm)	Qty per reel
SOT23-6	8	4	7"	280	160	3000

## 3. Others: NA



## **Revision History**

The revision history provided is for informational purpose only and is believed to be accurate, however, not warranted. Please make sure that you have the latest revision.

Date	Revision	Change		
Apr.20, 2023	Revision 1.0	Language improvements for clarity.		
June 20, 2021	Revision 0.9	Initial Release		



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