SA23003C

High-Efficiency, 5.5V, 3A, Single Synchronous Buck Converter

General Description

The SA23003C high efficiency 2.35MHz synchronous buck converter operates over an input voltage range of 2.8V to 5.5V and can deliver an output current up to 3A. It integrates a top MOSFET and a bottom MOSFET with very low $R_{DS(ON)}$ to minimize conduction loss. The 2.35MHz constant switching frequency reduces the required external inductor and capacitor values.

The SA23003C uses a peak current mode control architecture. It operates in fixed frequency pulse width modulation (PWM) mode at light to heavy loads, thereby maintaining small output voltage ripple over the entire load current range. It also provides cycle-by-cycle current limit protection, output short-circuit protection, and overtemperature protection.

The SA23003C is available in a compact DFN1.4mmx1.8mm-6 pin package.

Key Features

- 2.8V to 5.5V Input Voltage Range
- Up to 3A Output Current
- External Adjustable Voltage with ±1.5% Reference Accuracy
- 1µA Shutdown Current (Typical)
- Fixed 2.35MHz Switching Frequency
- Fixed Frequency PWM Operating Mode
- 100% Duty-Cycle Capable
- Cycle-by-Cycle Current Limit Protection
- Hiccup Mode Short-Circuit Protection
- Power Good Indicator
- Thermal Shutdown
- Compact DFN1.4×1.8-6 Package
- Automotive AEC-Q100 Grade 1 Certified

Applications

- Automotive Infotainment and Cluster
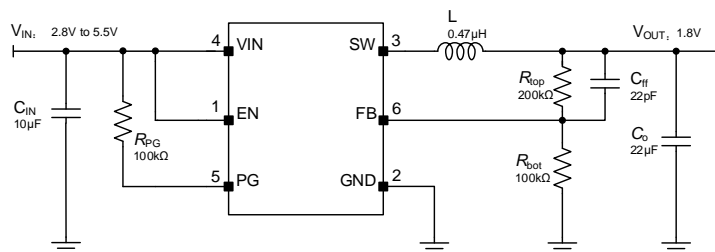- ADAS
- Automotive Display
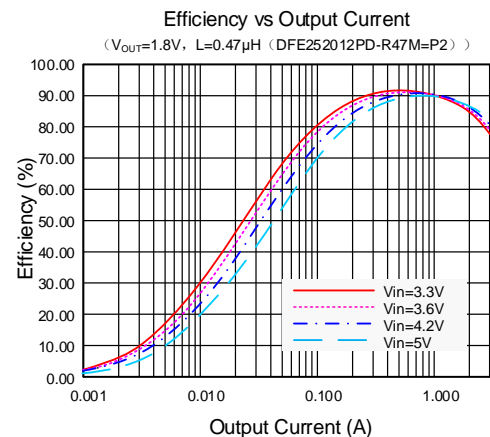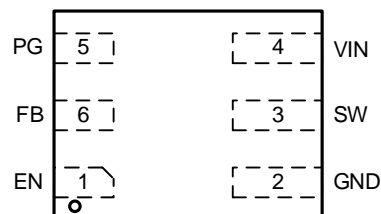- Other Electronic Equipment

Figure 1. Schematic Diagram

Figure 2. Efficiency vs Load Current

Ordering Information

Ordering Part Number	Package Type	Top Mark
SA23003CTWD	DFN1.4×1.8-6 RoHS-Compliant and Halogen-Free	**9m*xyz***

x = year code, y = week code, z = lot number code

Pinout (top view)

```
PG  [ 5 ]        [ 4 ]  VIN

FB  [ 6 ]        [ 3 ]  SW

EN  [ 1 ]        [ 2 ]  GND
```

(DFN1.4×1.8-6)

Pin Description

| Pin No	Pin Name	Pin Description
1	EN	Device enable pin, logic-high enable. There is no internal pulldown resistor. Do not leave floating.
2	GND	Ground
3	SW	Inductor pin. Connect this pin to the switching node of inductor.
4	VIN	Power input pin. Decouple this pin from the GND pin with at least a 10µF ceramic capacitor.
5	PG	Power good pin. Open-drain output. A pullup resistor is required (100kΩ, for example).
6	FB	Output voltage feedback pin. The output voltage reference is 0.6V.

Block Diagram
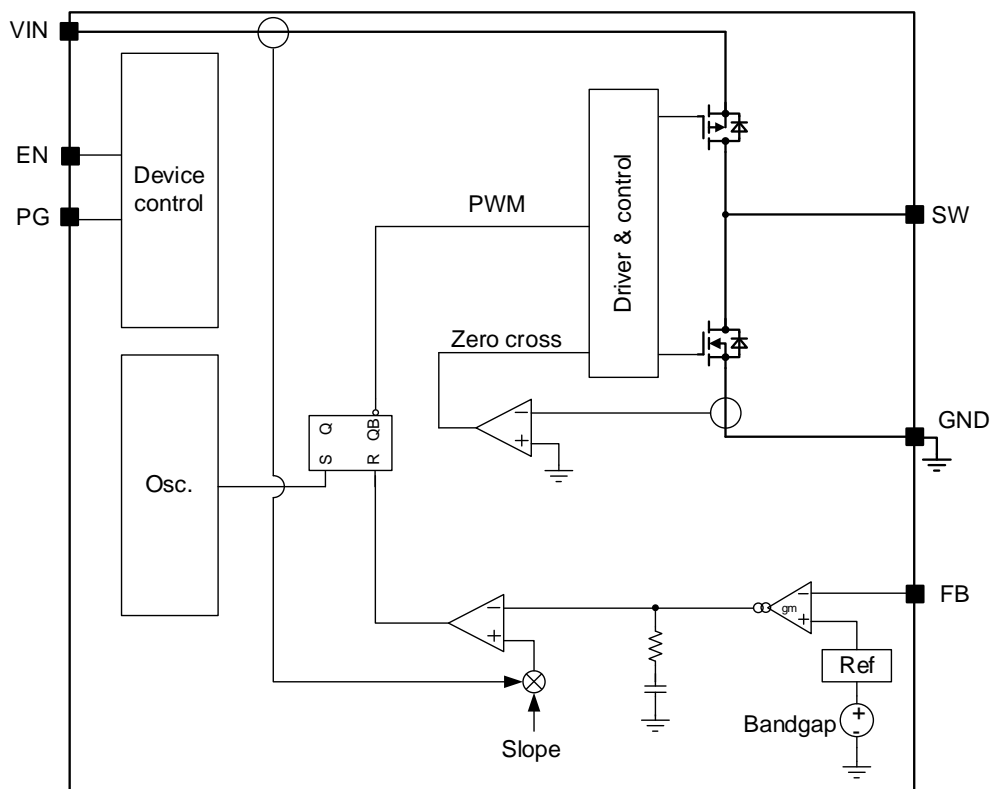
Figure 3. Functional Block Diagram

Absolute Maximum Ratings

Parameter (Note 1)	Min	Max	Unit
VIN	-0.3	6.5	
FB, EN, PG	-0.3	VIN + 0.3	V
Dynamic SW to GND Voltage in 20ns Duration	-3	VIN + 1.5	
Junction Temperature, Operating	-40	150	
Lead Temperature (Soldering, 10s)		260	°C
Storage Temperature	-65	150	
ESD Susceptibility			
HBM (Human Body Model)		2000	V
CDM (Charge Device Model) All Pins		500	

Thermal Information

Parameter (Note 2)	Typ	Unit
θ_{JA} Junction-to-Ambient Thermal Resistance	125	
θ_{JB} Junction-to-Board Thermal Resistance	69	°C/W
θ_{JC_TOP} Junction-to-Case Top Thermal Resistance	29	
Ψ_{JT} Junction-to-Top Characterization Parameter	4	
Parameter (Note 3)	**Typ**	**Unit**
θ_{JA} Junction-to-Ambient Thermal Resistance	60	
θ_{JB} Junction-to-Board Thermal Resistance	31	°C/W
θ_{JC_TOP} Junction-to-Case Top Thermal Resistance	29	
Ψ_{JT} Junction-to-Top Characterization Parameter	3	
P_D Power Dissipation @ T_A = 25°C	2.1	W

Recommended Operating Conditions

Parameter	Min	Max	Unit
VIN	2.8	5.5	V
Ambient Temperature	-40	125	°C
Junction Temperature	-40	150	

Electrical Characteristics

($2.8V \leq V_{IN} \leq 5.5V$, $-40°C \leq T_J \leq 125°C$. typical values at $V_{IN} = 5V$ and $T_J = 25°C$, unless otherwise noted)

Parameter		Symbol	Test Conditions	Min	Typ	Max	Unit
VIN	UVLO Rising Threshold	V_{UVLO_R}		2.6	2.7	2.8	V
	UVLO Falling Threshold	V_{UVLO_F}		2.45	2.55	2.65	
	Shutdown Current A	I_{SDA}	EN = 0V, $T_J = 25°C$		1	2	µA
	Shutdown Current B	I_{SDB}	EN = 0V, $T_J = 125°C$		6	12	
EN	EN Logic High Threshold	V_{EN_H}		1.2			V
	EN Logic Low Threshold	V_{EN_L}				0.4	
Power Stage	Switching Frequency	f_{SW}		2	2.35	2.7	MHz
	HS FET $R_{DS(ON)}$	$R_{DS(ON)\_HS}$	VIN = 5V		83		mΩ
	LS FET $R_{DS(ON)}$	$R_{DS(ON)\_LS}$	VIN = 5V		43		
	Discharge Resistor	$R_{DISCHARGE}$			200		Ω
Feedback and Soft-Start	Output Feedback Reference	V_{REF}		591	600	609	mV
	Soft-Start Time	t_{ss}	Output from 10% to 90%	0.2	0.4	1	ms
Power Good	Falling (Fault) Voltage	V_{PGTH_FF}	V_{FB} as percent of V_{REF}	80	85	90	%
	Rising (Good) Voltage	V_{PGTH_RG}	V_{FB} as percent of V_{REF}	85	90	95	%
	Rising (Fault) Voltage	V_{PGTH_RF}	V_{FB} as percent of V_{REF}	110	115	120	%
	Falling (Good) Voltage	V_{PGTH_FG}	V_{FB} as percent of V_{REF}	105	110	115	%
	Delay Time	t_{PG_DELAY}			17		µs
Thermal Shutdown	Thermal Shutdown Threshold	T_{SD}		150	165	180	°C
	Thermal Shutdown Hysteresis	T_{SDHYS}		10	15	20	
Current Limit	Peak Current Limit	I_{LIMIT_P}		4.0	5.0	6.0	A
	Valley Foldback Current Limit	I_{LIMIT_V}		2.3	3.5	4.5	
	Negative Valley Current Limit	I_{LIMIT_N}		1	1.6	2.2	
Short-Circuit Protection	Short-Circuit Threshold	V_{SCP}	V_{FB} as percent of V_{REF}	20	30	40	%
	Short-Circuit Response Time	t_{SCP}	From $V_{FB} < V_{SCP}$ to stop switching. No delay on the other side, $V_{IN} = 5V$.	5	10	20	µs

Note 1: Stresses beyond the "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only. Functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.
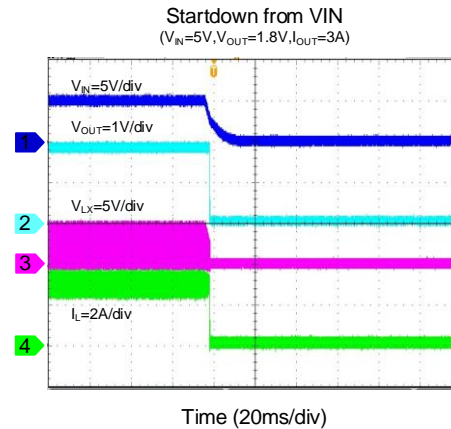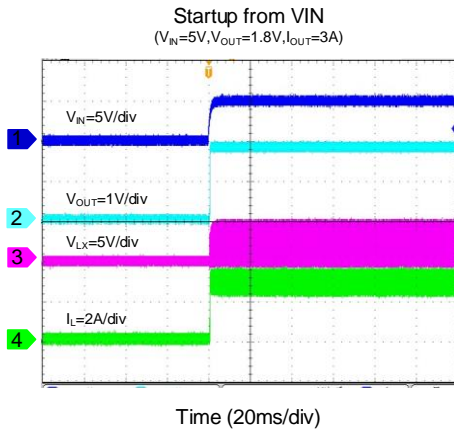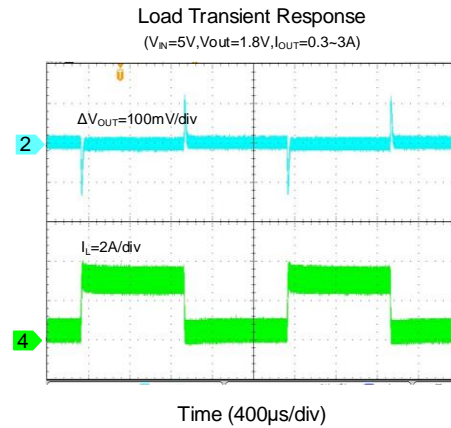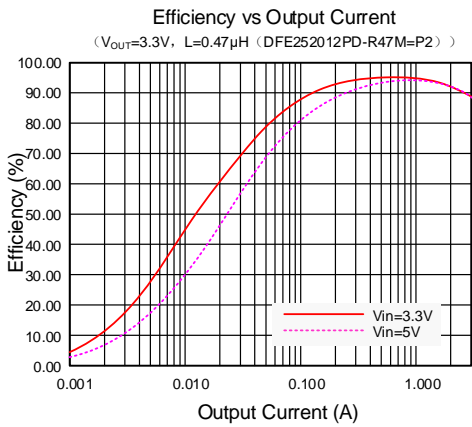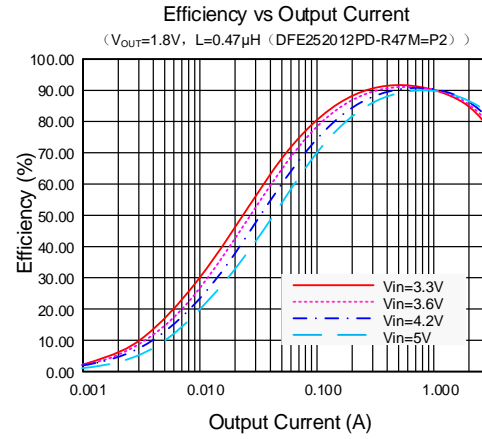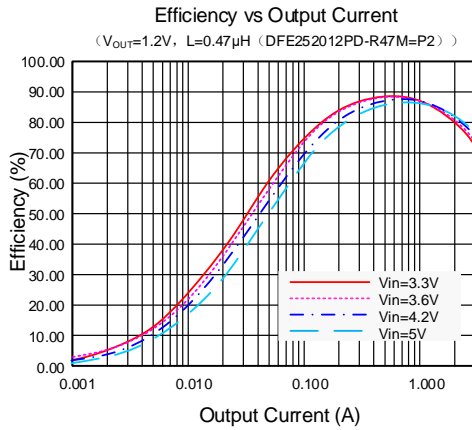
Note 2: The parameters are measured in the natural convection at $T_A = 25°C$. Device mounted on 4-layer test board of JESD51-7 thermal measurement standard.

Note 3: The parameters are measured in the natural convection at $T_A = 25°C$. Device mounted on Silergy 4-layer, 6" x 6" FR-4 substrate PCB, 1oz copper, with minimum recommended pad on top layer and thermal vias to bottom layer ground plane.
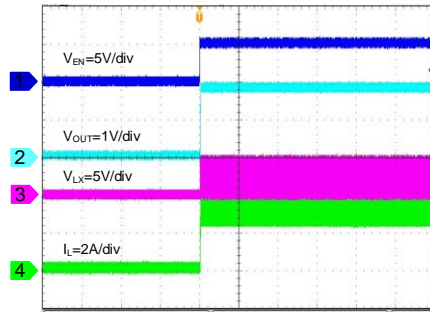
Note 4: The device is not guaranteed to function outside its operating conditions.

Typical Performance Characteristics

(T_A = 25°C, VIN = 5V, V_{OUT} =1.8V, L = 0.47µH, C_{OUT} = 22µF, unless otherwise noted)

Efficiency vs Output Current
（V_{OUT}=1.2V，L=0.47µH（DFE252012PD-R47M=P2））

Efficiency vs Output Current
（V_{OUT}=1.8V，L=0.47µH（DFE252012PD-R47M=P2））

Efficiency vs Output Current
（V_{OUT}=3.3V，L=0.47µH（DFE252012PD-R47M=P2））

Load Transient Response
(V_{IN}=5V,Vout=1.8V,I_{OUT}=0.3~3A)

Startup from VIN
(V_{IN}=5V,V_{OUT}=1.8V,I_{OUT}=3A)

Startdown from VIN
(V_{IN}=5V,V_{OUT}=1.8V,I_{OUT}=3A)

Startup from VEN
(V$_{IN}$=5V,V$_{OUT}$=1.8V,I$_{OUT}$=3A)

V$_{EN}$=5V/div

V$_{OUT}$=1V/div

V$_{LX}$=5V/div

I$_L$=2A/div

Time (10ms/div)

Startdown from VEN
(V$_{IN}$=5V,V$_{OUT}$=1.8V,I$_{OUT}$=3A)

V$_{EN}$=5V/div

V$_{OUT}$=1V/div

V$_{LX}$=5V/div

I$_L$=2A/div

Time (10ms/div)

Output Ripple
(V$_{IN}$=5V,V$_{OUT}$=1.8V,I$_{OUT}$=0A)

ΔV$_{OUT}$=20mV/div

V$_{LX}$=5V/div

I$_L$=500mA/div

Time (40ms/div)

Output Ripple
(V$_{IN}$=5V,V$_{OUT}$=1.8V,I$_{OUT}$=3A)

ΔV$_{OUT}$=10mV/div

V$_{LX}$=5V/div

I$_L$=2A/div
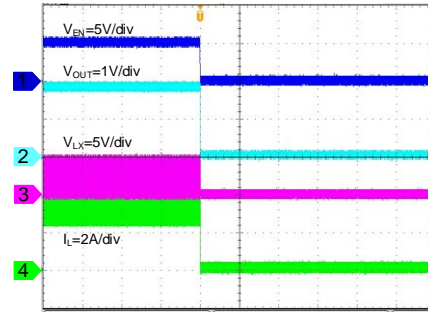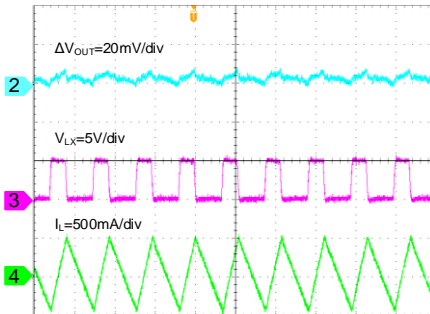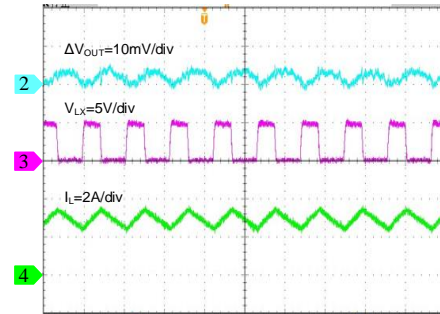
Time (400ns/div)

Output Short Circuit
(V$_{IN}$=5V,V$_{OUT}$=1.8V,I$_{OUT}$=0A)

V$_{OUT}$=1V/div

I$_L$=2A/div
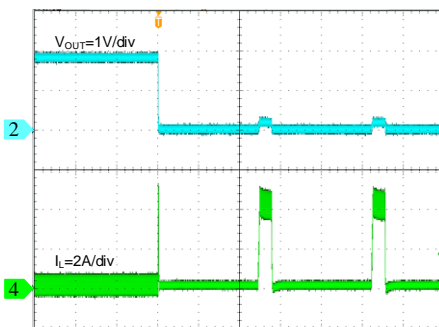
Time (2ms/div)

Output Short Circuit
(V$_{IN}$=5V,V$_{OUT}$=1.8V,I$_{OUT}$=3A)

V$_{OUT}$=1V/div

I$_L$=2A/div

Time (2ms/div)

Bode Plot
(V_{IN} = 5V, V_{OUT} = 1.2V, I_{OUT} = 3A)

Red Cursor Information:
Band Width: 221.14 kHz
Phase Margin: 71.69 deg

Blue Cursor Information:
Frequency: 708.335kHz
Gain: -13.54 dB

Bode Plot
(V_{IN} = 5V, V_{OUT} = 1.8V, I_{OUT} = 3A)

Red Cursor Information:
Band Width: 227.93kHz
Phase Margin: 63.84 deg

Blue Cursor Information:
Frequency: 618.3 kHz
Gain: -10.3 dB

Bode Plot
(V_{IN} = 5V, V_{OUT} = 3.3V, I_{OUT} = 3A)

Red Cursor Information:
Band Width: 231.774kHz
Phase Margin: 51.36 deg

Blue Cursor Information:
Frequency: 467.5 kHz
Gain: -10.05 dB

IQ_No load VS Temperature
(V_{IN}=5V, V_{OUT}=1.8V, I_{OUT}=0A)

Detailed Description

General Description
The SA23003C high efficiency 2.35MHz synchronous buck converter operates over an input voltage range of 2.8V to 5.5V and can deliver an output current up to 3A. It integrates a top MOSFET and a bottom MOSFET with very low $R_{DS(ON)}$ to minimize conduction loss. The 2.35MHz constant switching frequency reduces the required external inductor and capacitor values.

The SA23003C also provides cycle-by-cycle current limit protection, output short-circuit protection, and overtemperature protection.

Peak Current Mode Control
The SA23003C uses a fixed frequency peak current mode control architecture. The peak current through the high-side (HS) MOSFET is added to the slope compensation ramp and fed into the positive input of the PWM comparator. The output voltage is also sensed through an external feedback resistor divider network and fed into the error amplifier negative input. The output of the error amplifier is fed into the negative input of the PWM comparator. At the start of any switching cycle, the oscillator sets the RS latch by using the switch logic block. This forces a high signal on the gate of the high side MOSFET, turning it on. When the voltage on the positive input of the PWM comparator exceeds the negative input, the RS latch is reset and the high side MOSFET turns off and after a short time the low-side (LS) MOSFET turns on.

ON-OFF Sequence
The normal startup of the chip is determined by two factors. First, the EN pin level must exceed the logic high level threshold. Second, the voltage present at VIN pin must exceed the UVLO rising threshold. After the EN pin level is set high, whether the chip is turned on is determined by the voltage of the VIN pin. When both conditions are met, the internal reference voltage starts ramping and the device starts operating. After a 300µs delay, the soft-start circuit is enabled and the SW node begins switching. After a fixed soft-start time t_{SS} (0.4 ms typ.), the output reaches the target value.
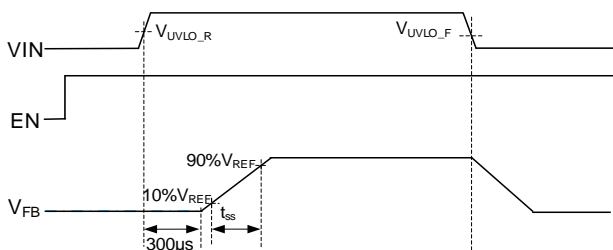

Figure 4. VIN ON/OFF Sequence

When the VIN pin voltage is higher than 2.7V (typical), the EN pin voltage determines whether the chip begins operating. Once the EN pin voltage is above the logic high level, the internal reference voltage begins to build and the functional circuit begins operating. After a 300µs delay, the soft-start circuit begins operating and the SW node begins switching. After a fixed soft-start time, the output reaches the target value.
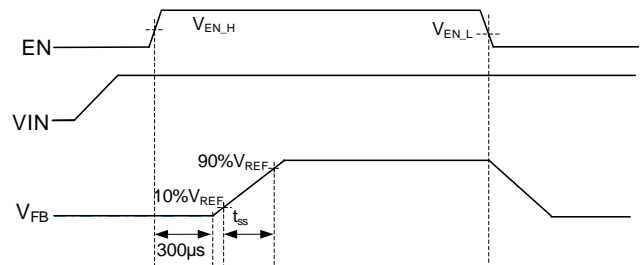

Figure 5. EN ON/OFF Sequence

Adaptive Frequency Foldback at Minimum T_{OFF} Operation (Dropout)
The SA23003C provides adaptive frequency reduction during large-duty-cycle operation when minimum T_{OFF} is reached. Unlike conventional peak current control, this approach ensures the stability of the circuit during dropout operation. When V_{IN} drops below the configured V_{OUT} voltage, the SA23003C will enter dropout mode, wherein its high side MOSFET will always be on. Normal operation resumes when V_{IN} exceeds the target V_{OUT} level.

Power Good
The SA23003C provides an open-drain output controlled by a window comparator for power good indication. The PG pin is driven low until the internal soft-start is complete. When the FB pin voltage raises above V_{PGTH_RG} and stays above V_{PGTH_FG}, the PG pin is high-impedance, and the output is pulled high by the external resistor connected to a voltage source. In addition, when the FB pin voltage exceeds V_{PGTH_FF} and stays above V_{PGTH_RF}, the open-drain MOSFET turns on and the PG pin is pulled low.

A pullup resistor value of 2kΩ to 100kΩ is recommended for the power source.
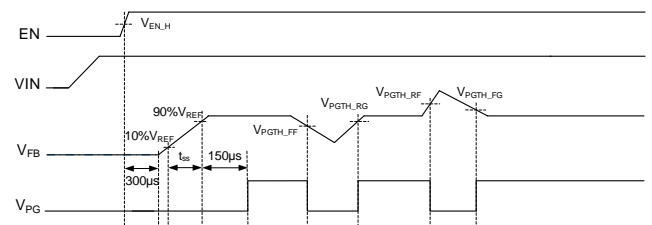

Figure 6. Power Good Logic

This pin can be connected to GND or left unconnected if not used. .

Soft-Start

The SA23003C features soft-start to ensure moderate inrush current and reduce output overshoot. The soft-start circuit charges a capacitor with a fixed current to ramp up the reference voltage. The soft-start time is fixed by an internal capacitor.

Table 1. Soft-Start

Parameter	Symbol	Test Conditions	Min	Typ	Max	Unit
Soft-Start Time	t_{SS}	Output from 10% to 90%		0.4		ms
Startup Delay Time	t_{DELAY}	Time from EN high to soft-start		300		µs

Fault Protection Modes

The SA23003C provides integrated output short-circuit protection, output overcurrent protection, and thermal shutdown protection.

Table 2. Fault Protection Modes

Protection	Threshold	Deglitch Time	Operation
Thermal Shutdown	Rising: 165°C Falling: 150°C	-	Shutdown when temperature > 165°C Restart when temperature<150°C
Cycle-by-Cycle Current Limit	5A		Peak limit = valley limit. Valley Foldback to 70% after 3 cycles.
Output SCP	$V_{FB}<30\%V_{REF}$	10µs	Hiccup time 5.5ms.

Cycle-by-Cycle Current Limit Protection

The SA23003C features cycle-by-cycle current limit protection. The internal high side and low side MOSFET current sense signals and peak/valley current limit reference voltages are fed to the positive and negative inputs of the current limiting comparator, respectively. When V_{FB} exceeds V_{SCP} and peak current limits are detected for three consecutive cycles, the valley current limit reference will be reduced, thus avoiding minimum T_{ON} operation and reducing the heat dissipation.
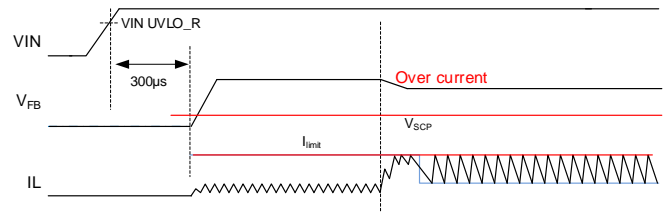

Figure 7. Cycle-by-Cycle Current Limit

Short-Circuit Protection

The SA23003C provides output short-circuit protection to prevent power MOSFETs damage. When the output voltage is short-circuited and the FB voltage is lower than the short-circuit threshold voltage V_{SCP}, the chip will turn off the high side and low side MOSFETs and enter hiccup mode until the fault is removed.
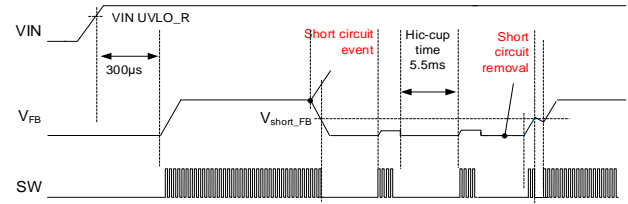

Figure 8. Short-Circuit Protection

Overtemperature Protection

The SA23003C enters thermal shutdown when the junction temperature exceeds 165°C (typical). In this mode, both MOSFETs are turned off. When the junction temperature falls below 150°C (typical), the buck converter will automatically restart and initiate a soft-start.
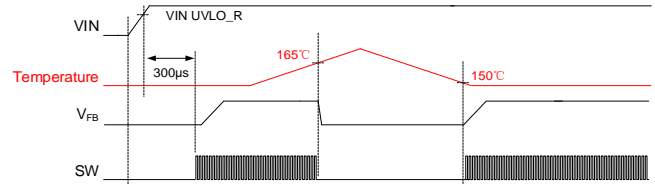

*Figure 9. Overtemperature Protection*

Application Information

The following paragraphs provide information on the selection of the external components needed to meet the targeted application specifications.

Feedback Resistor Dividers R_TOP and R_BOT

Choose R_TOP and R_BOT to program the proper output voltage. Choose resistance values between 10kΩ and 1MΩ for both R_TOP and R_BOT to minimize power consumption under light loads. In order to achieve better load transient performance and phase margin, refer to the Typical Application section for recommended feedback resistor values.

The output voltage can be configured using the following equation:

$$V_{OUT} = \left(1 + \frac{R_{TOP}}{R_{BOT}}\right) \times V_{FB}$$
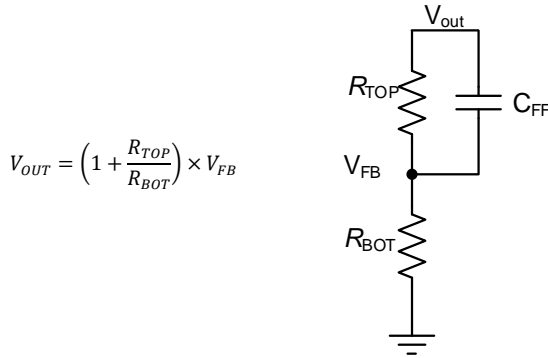
where V_FB has a value of 0.6V (typical).

Output Inductor L

Consider the following when choosing this inductor:

1) Choose the inductance to provide a ripple current that is approximately 40% of the maximum output current. The recommended inductance is calculated as:

$$L = \frac{V_{OUT}(1 - V_{OUT}/V_{IN,MAX})}{f_S \times I_{OUT,MAX} \times 0.4}$$

where f_S is the switching frequency and $I_{OUT,MAX}$ is the maximum load current.

The SA23003C has high tolerance for ripple current amplitude variation. As a result, the final choice of inductance can vary slightly from the calculated value with no significant performance impact.

2) The inductor's saturation current rating must be greater than the peak inductor current under full load:

$$I_{SAT\_MIN} > I_{OUT\_MAX} + \frac{V_{OUT}(1 - V_{OUT}/V_{IN,MAX})}{2f_S \times L}$$

3) The DCR of the inductor and the core loss at the switching frequency must be low enough to achieve the desired efficiency. Choose an inductor with smaller DCR to achieve a good overall efficiency.

Input Capacitor C_IN

Input filter capacitors are needed to reduce the ripple voltage on the input, to filter the switched current drawn from the input supply, and to reduce EMI. When selecting the input capacitor, be sure to select a voltage rating at least 20% greater than the maximum voltage of the input supply, and a temperature rating above the system requirements. X7R series ceramic capacitors are most often selected due to their surge current capability and high RMS current ratings over a wide temperature and voltage range. Systems that are powered by a wall adapter or a long inductive cable may be susceptible to significant inductive ringing at the input of the device. In these cases, consider adding some bulk capacitance like electrolytic, tantalum, or polymer type capacitors. Using a combination of bulk capacitors (to reduce input overshoot or ringing) in parallel with ceramic capacitors (to meet the RMS current requirements) is helpful in these cases.

Consider the RMS current rating of the input capacitor, paralleling additional capacitors if required to meet the calculated RMS ripple current

$$I_{CIN\_RMS} = I_{OUT} \times \sqrt{D \times (1 - D)}$$

The worst-case condition occurs at D = 0.5, then

$$I_{CIN\_RMS,MAX} = \frac{I_{OUT}}{2}$$

For simplicity, choose an input capacitor with an RMS current rating greater than half of the maximum load current.

The input capacitance value determines the input voltage ripple of the converter. If there is an input voltage ripple requirement in the system, choose an appropriate input capacitor that meets the specification. Given the very low ESR and ESL of ceramic capacitors, the input voltage ripple can be estimated as follows:

$$V_{CIN\_RIPPLE,CAP} = \frac{I_{OUT}}{f_{SW} \times C_{IN}} \times D \times (1 - D)$$

The worst-case condition occurs at D = 0.5, then

$$V_{CIN\_RIPPLE,CAP,MAX} = \frac{I_{OUT}}{4 \times f_{SW} \times C_{IN}}$$

The capacitance value is less important than the RMS current rating. In most applications, a single 10µF(0603) X7R capacitor is sufficient. Place the ceramic input capacitor as close to the device's VIN and GND pins as possible.

Output Capacitor C_OUT

Select the output capacitor C_OUT to handle the output ripple requirements. Both steady-state ripple and transient requirements must be taken into consideration when selecting C_OUT. It is recommended to use an X7R or better grade ceramic capacitor (refer to the Typical

Application section for recommended capacitance values).

For applications where the design must meet stringent ripple requirements, the following considerations must be followed:

The output voltage ripple at the switching frequency is caused by the inductor current ripple (ΔI_L) on the output capacitor's ESR (ESR ripple), as well as the stored charge (capacitive ripple). When calculating total ripple, consider both.

$$V_{RIPPLE,ESR} = \Delta I_L \times ESR$$

$$V_{RIPPLE,CAP} = \frac{\Delta I_L}{8 \times C_{OUT} \times f_{SW}}$$

The measured capacitive ripple may be higher than the calculated value because the effective capacitance for ceramic capacitors decreases with the voltage across their terminals. The voltage derating is usually included as a chart in the capacitor datasheet, and the ripple can be recalculated after taking the target output voltage into account. The recommended minimum output capacitance values for typical applications are provided below, based on the Vout selected.

Feedforward Capacitor C_{FF}

The device integrates the compensation components to achieve good stability and fast transient responses. In applications with high load steps, adding a ceramic capacitor (feedforward capacitor C_{FF}) in parallel with R_H may help speed up the load transient response. A value between 22 pF and 47 pF is recommended for most applications.

Refer to the Typical Application section for the recommended values.
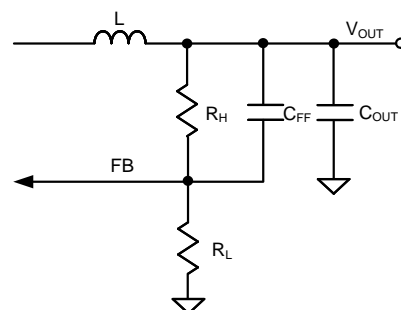
Application Schematic $(V_{OUT} = 1.8V)$
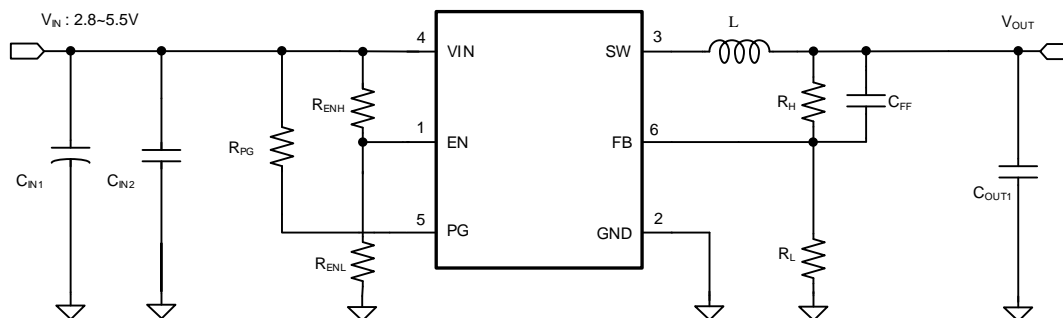
BOM List

Reference Designator	Description	Part Number	Manufacturer
C_{IN1}	47µF/50V Electrolytic Capacitor		
C_{IN2}	10µF/6.3V/X7T, 0603	GCM188D70J106ME36D	muRata
C_{OUT1}	22µF/6.3V/X7T, 0603	GRM188D70J226ME01D	muRata
L	0.47µH/inductor, 5.2A	DFE252012PD-R47M=P2	muRata
C_{FF}	22pF/50V/C0G, 0603		
R_H	200kΩ, 1%, 0603		
R_L	100kΩ, 1%, 0603		
R_{PG}	100kΩ, 1%, 0603		
R_{ENH}	10kΩ, 1%, 0603		
R_{ENL}	1MΩ, 1%, 0603		

Recommended Component Values for Typical Applications

V_{OUT} (V)	R_H (kΩ)	R_L (kΩ)	C_{FF} (pF)	L/Part Number	C_{OUT}
0.6	0	NC	NC	0.47µH/DFE252012PD-R47M=P2	22µF*2/6.3V, 0603, X7T
0.85	49.9	120	47	0.47µH/DFE252012PD-R47M=P2	22µF/6.3V, 0603, X7T
1.2	100	100	22	0.47µH/DFE252012PD-R47M=P2	22µF/6.3V, 0603, X7T
1.8	200	100	22	0.47µH/DFE252012PD-R47M=P2	22µF/6.3V, 0603, X7T
3.3	270	60.4	47	0.47µH/DFE252012PD-R47M=P2	22µF/6.3V, 0603, X7T

Layout Design

Follow these PCB layout guidelines for optimal performance and thermal dissipation:

- **Input Capacitors:** Place the input capacitors as close as possible to the VIN and GND pins, minimizing the loop formed by these connections. The input capacitor should be connected to the VIN and GND pins using wide copper areas.

- **Output Capacitors:** Connect the C_{OUT} negative terminal to the GND pin using wide copper traces instead of vias, in order to achieve better accuracy and stability of the output voltage.

- **Feedback Network:** Place the feedback components (R_H, R_L, and C_{FF}) as close to the FB pin as possible. Avoid routing the feedback line near SW or other high frequency signals as it is noise-sensitive. Use a Kelvin connection to connect with C_{OUT} rather than the inductor output terminal.

- **SW Connection:** Keep the SW area small to prevent excessive EMI, while providing a wide copper trace to minimize parasitic resistance and inductance.

- **EN Signal:** It is not recommended to connect the EN pin directly to VIN. A resistor in the range of 1kΩ to 1MΩ should be used if EN pin is pulled high to VIN voltage.

- **GND Vias:** Place an adequate number of vias on the GND layer around the device for better thermal performance.

- **PCB Board:** To achieve the best thermal and noise performance, maximize the PCB copper area connecting to the GND pin. A ground plane is highly recommended if possible. Connect the ground pad to a large copper area to enhance thermal performance.
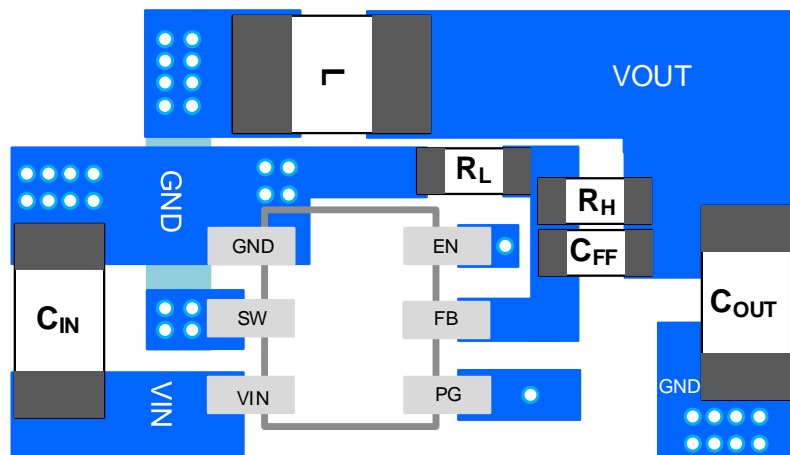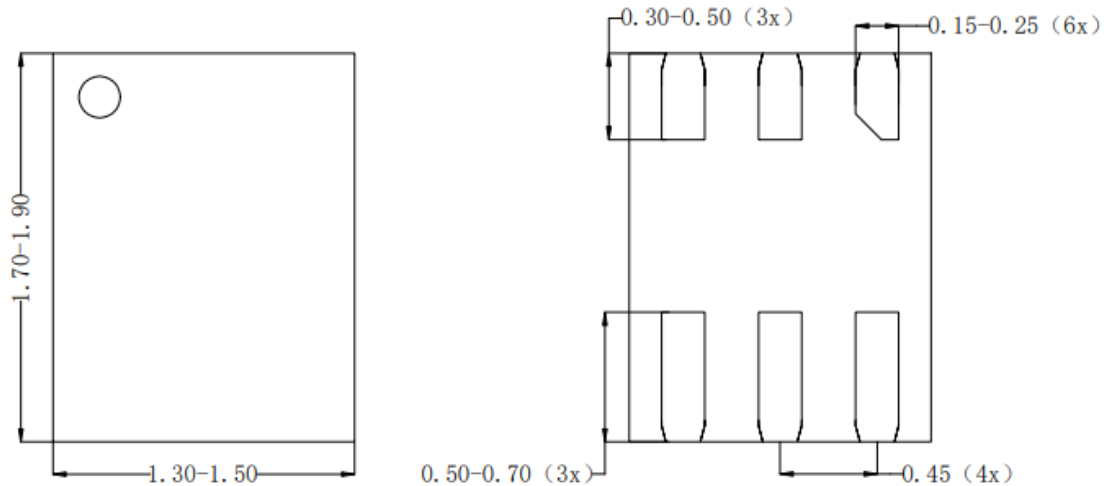

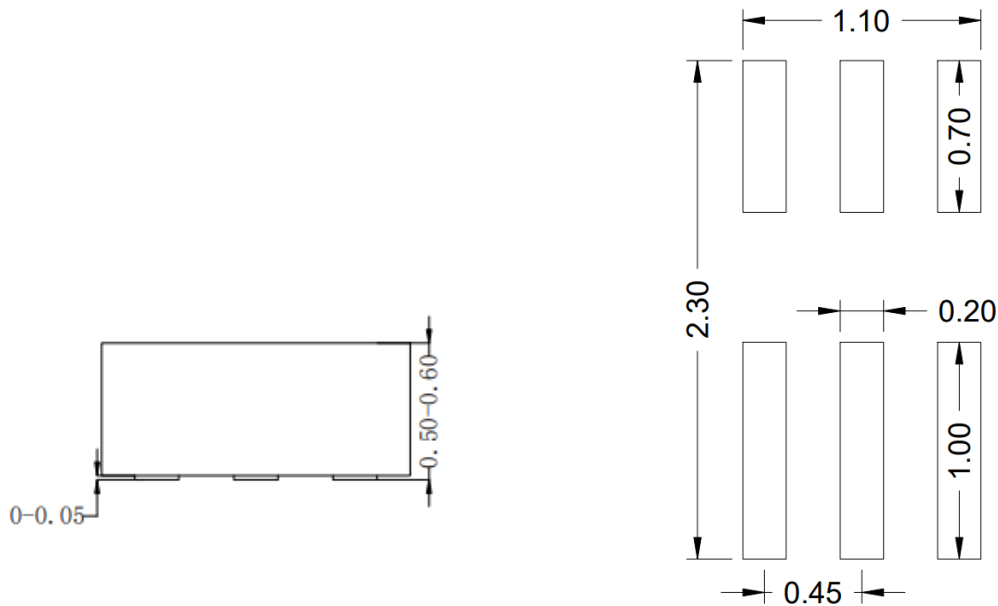*Figure 10. Suggested PCB Layout*

DFN1.4×1.8-6 Package Outline Drawing
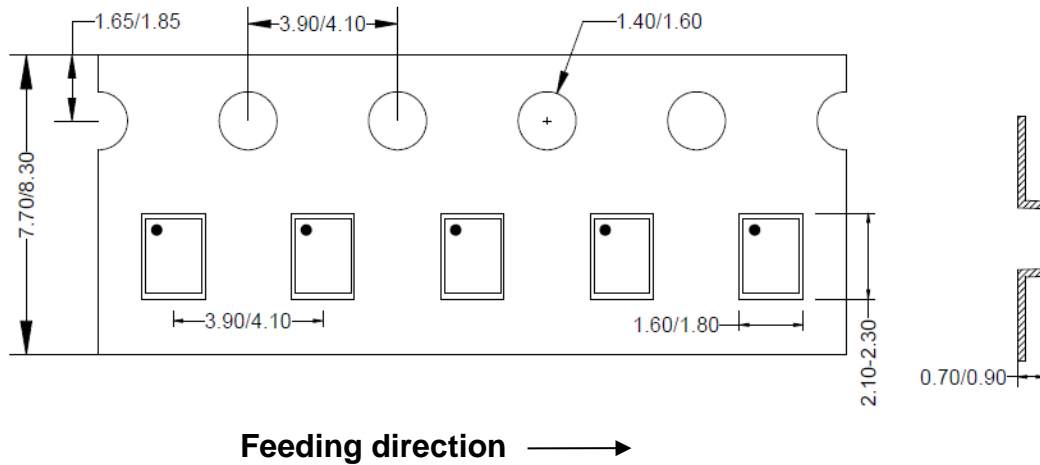
Top View

Bottom view

Side View

Recommended PCB layout (Reference only)

Notes: All dimensions are in millimeters and exclude mold flash and metal burr.

Tape and Reel Specification

DFN1.4×1.8 Tape Orientation

Feeding direction ⟶

Carrier Tape and Reel Specification for Packages
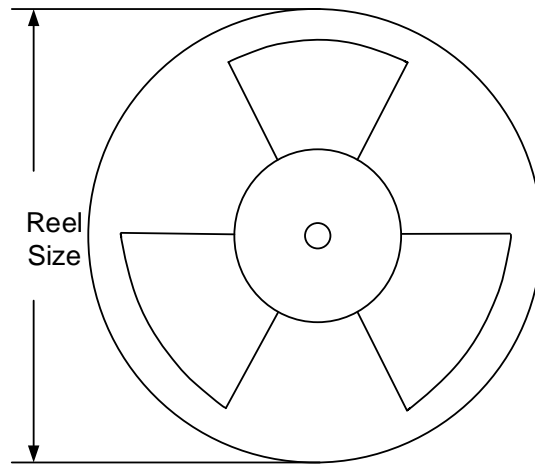
Package Types	Tape Width (mm)	Pocket Pitch (mm)	Reel Size (inch)	Trailer Length (mm)	Leader Length (mm)	Qty per Reel
DFN1.4×1.8	8	4	7"	400	400	3000

Revision History

The revision history provided is for informational purpose only and is believed to be accurate, however, not warranted. Please make sure that you have the latest revision.

Date	Revision	Change	Pages changed
Apr. 24, 2024	Revision 1.0	Initial Release	-

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