

### SY21061 High Efficiency, 800kHz, 1.2A, 40V Input Asynchronous Buck Converter

### **General Description**

The SY21061 high-efficiency asynchronous Buck converter can deliver 1.2A output current over a wide input voltage range from 5V to 40V. The SY21061 employs a constant off-time and peak current mode control strategy to achieve fast transient responses. It integrates a main switch with low  $R_{DS(ON)}$  to minimize conduction loss.

The 800kHz switching frequency permits low output voltage ripple and reduces external inductor and capacitor sizes. The SY21061 also provides cycle-by-cycle current limiting, over temperature protection, and output short circuit protection.

The SY21061 is available in a compact SOT23-6 package.

#### Features

- Low  $R_{\text{DS(ON)}}$  for Internal N-channel Power FET: 180m $\Omega$
- 5V to 40V Input Voltage Range
- Up to 1.2A Output Current
- 800kHz Switching Frequency
- Constant Off-Time and Peak Current Mode Control
- Internal Soft-Start Limits Inrush Current
- ±2% 0.6V Reference
- Output Short Circuit Protection
- Cycle-by-Cycle Peak Current Limit
- Over Temperature Protection
- RoHS-Compliant and Halogen-Free
- Compact SOT23-6 Package

### Applications

- Smart Meter
- Set Top Box
- Portable TV
- Access Point Router

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- DSL Modem
- LCD TV

### **Typical Application**

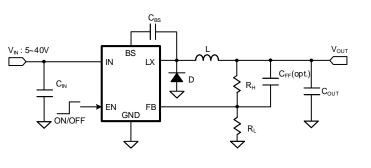
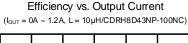


Figure 1. Typical Application Circuit



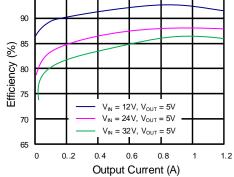


Figure 2. Efficiency vs. Output Current

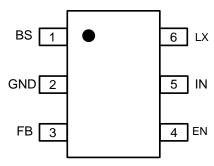


# **Ordering Information**

Ordering Part Number	Package type	Top Mark		
SY21061ABC	SOT23-6 RoHS-Compliant and Halogen- Free	YM <i>xyz</i>		
x - vear code, x - week code, z - lot number code				

x = year code, y = week code, z = lot number code

## Pinout (top view)



# **Pin Description**

Pin No	Pin Name	Pin Description
1	BS	Bootstrap pin. Supply for high-side gate driver. Connect a 0.1µF ceramic capacitor between the BS and LX pin.
2	GND	Ground pin.
3	FB	Output feedback pin. Connect this pin to the center point of the output resistor-divider as shown in Figure 1. $V_{OUT} = 0.6 \times (1 + R_H/R_L)$ .
4	EN	Enable pin. Pull low to disable the device, pull high to enable. Do not leave this pin floating.
5	IN	Power input. Decouple this pin from the GND pin with at least a $2.2\mu$ F ceramic capacitor.
6	LX	Inductor pin. Connect this pin to the switching node of inductor and rectifier diode.



# **Block Diagram**

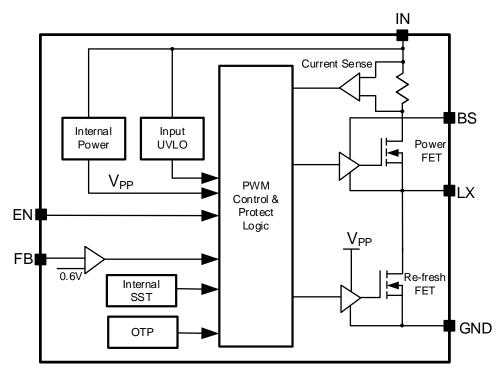


Figure 3. Block Diagram

# **Absolute Maximum Ratings**

Parameter (Note 1)	Min	Max	Unit
IN, LX	-0.3	42	
EN	-0.3	V <sub>IN</sub> + 0.6	V
FB, BS-LX	-0.3	3.6	
Junction Temperature, Operating	-40	150	
Lead Temperature (Soldering, 10sec.)		260	°C
Storage Temperature	-65	150	

## **Thermal Information**

Parameter (Note 2)	Тур	Unit
θ <sub>JA</sub> Junction-to-ambient Thermal Resistance	170	°C/W
θ <sub>JC</sub> Junction-to-case Thermal Resistance	130	C/VV
P <sub>D</sub> Power Dissipation T <sub>A</sub> =25°C	0.6	W

## **Recommended Operating Conditions**

Parameter (Note 3)	Min	Max	Unit
IN	5	40	V
BS-LX		3.3	v
Output Current		1.2	А
Junction Temperature	-40	125	ŝ
Ambient Temperature	-40	85	C



# **Electrical Characteristics**

Parameter		Symbol	Test Conditions	Min	Тур	Max	Unit
	Voltage Range	Vin		5		40	V
	UVLO Rising Threshold	Vin,uvlo	Rising		4.5		v
Input	UVLO Hysteresis	VIN, HYS			200		mV
Input	Quiescent Current	lq	Iout = 0A, Vfb = Vref×105%		160		μA
	Shutdown Current	ISHDN	EN = Low			10	-
	Reference Voltage	VREF		0.588	0.6	0.612	V
Output	FB input Current	I <sub>FB</sub>	$V_{FB} = V_{IN}$	-50		50	nA
	Soft-Start Time	tss	(Note 4)		400		μs
MOSELL	Power FET RDS(ON)	RDS(ON)			180		mΩ
MOSFET	Power FET Current Limit	ILIM	$V_{FB} = V_{REF} \times 98\%$	1.6		2	А
Enable (EN)	Input Voltage High	V <sub>EN,H</sub>		1.5			V
Enable (EN)	Input Voltage Low	V <sub>EN,L</sub>				0.4	V
	Switching Frequency	fsw			800		kHz
Fraguanay	Minimum On-time	ton,min	(Note 4)			100	ns
Frequency	Maximum On-time	ton,max			2		μs
	Minimum Off-time	toff,min				100	ns
OTP	Temperature	Тотр	(Note 4)		150		°C
	Temperature Hysteresis	THYS	(Note 4)		15		C

**Note 1**: Stresses beyond the "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only. Functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

**Note 2**:  $\theta_{JA}$  is measured in the natural convection at  $T_A = 25^{\circ}$ C on a low effective single layer thermal conductivity test board of JEDEC 51-3 thermal measurement standard.

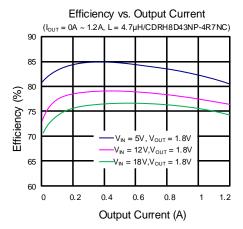
**Note 3:** The device is not guaranteed to function outside its operating conditions.

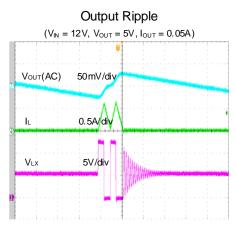
Note 4: Guaranteed by design.



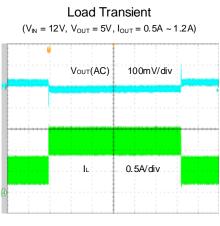
# **Typical Performance Characteristics**

 $(T_A = 25^{\circ}C, V_{IN} = 12V, V_{OUT} = 5V, L = 10\mu$ H,  $C_{OUT} = 22\mu$ F, unless otherwise specified)

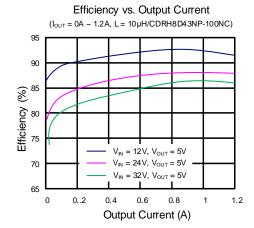


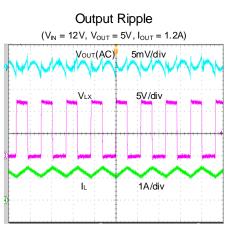


Time (2µs/div)



Time (800µs/div)

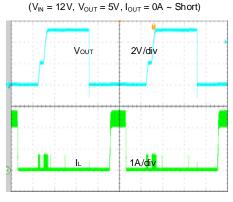




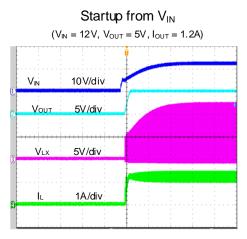
Time (1µs/div)



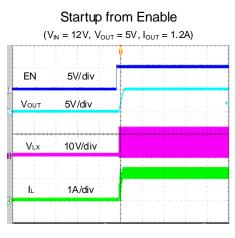
Short Circuit Protection



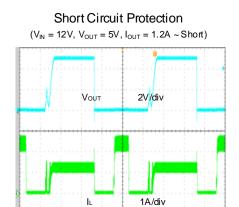
#### Time (2ms/div)



Time (2ms/div)

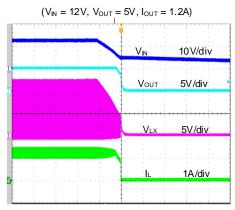


Time (2ms/div)

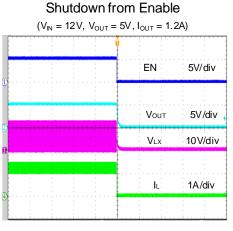


Time (2ms/div)

Shutdown from V<sub>IN</sub>

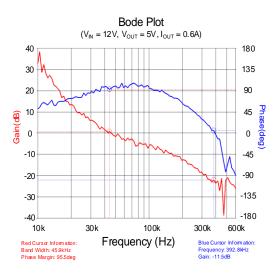


Time (2ms/div)



Time (2ms/div)







## **Detailed Description**

The SY21061 high-efficiency asynchronous Buck converter can deliver 1.2A output current over a wide input voltage range from 5V to 40V. It integrates a power FET with low  $R_{DS(ON)}$  to minimize conduction loss.

The 800kHz switching frequency permits low output voltage ripple and reduces external inductor and capacitor sizes. The SY21061 also provides cycle-by-cycle current limiting, over temperature protection and output short circuit protection.

The SY21061 employs a constant off-time and peakcurrent mode control strategy. When the power FET's current-sense signal reaches internal  $V_{COMP}$ , the power FET turns off for a fixed period of time (constant off-time). t<sub>OFF</sub> is internally calculated according to the input voltage, output voltage, and desired switching frequency (f<sub>SW</sub>):

$$t_{OFF} = \frac{1 - V_{OUT} / V_{IN}}{f_{SW}}$$

The power FET turns on after a period of t<sub>OFF</sub>.

#### **Enable Control**

The EN input is a high-voltage capable input with logiccompatible threshold. When EN is driven higher than 1.5V, normal device operation is enabled. When driven to lower than 0.4V, the device will shut down, reducing input current to less than  $10\mu$ A.

### **Fault-Protection Modes**

#### **Output Current Limit**

With load current increasing, as soon as the power FET current exceeds the peak current-limit threshold, the power FET will turn off. If the load current continues to increase, the output voltage will drop.

#### **Output Under Voltage Protection**

With output current increasing, as soon as the power switch current exceeds the peak current limit threshold, the power switch will turn off. If the load current continues to increase, the output voltage will drop. When the output voltage falls below 33% of the regulated level, the output undervoltage protection will be activated and the device will operate in hiccup mode. The hiccup on-time is 1.5ms, and the hiccup off-time is 1.5ms. If the hard short condition is removed, the device will return to normal operation.

#### **Overtemperature Protection (OTP)**

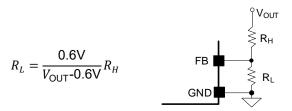
The device includes overtemperature protection (OTP) circuitry to prevent overheating due to excessive power dissipation. This will shut down the device when the junction temperature exceeds 150°C. Once the junction temperature cools by approximately 15°C, the device will resume normal operation after a complete soft-start cycle. For continuous operation, provide adequate cooling so that the junction temperature does not exceed the OTP threshold.

## **Application Information**

The following paragraphs describe the selection process for the feedback resistors ( $R_H$  and  $R_L$ ), input capacitor  $C_{IN}$ , output inductor L, output capacitor  $C_{OUT}$ , bootstrap capacitor and rectifier diode D.

#### Feedback Resistor-Divider R<sub>H</sub> and R<sub>L</sub>

Choose  $R_H$  and  $R_L$  to program the proper output voltage. Choose large resistance values between  $10k\Omega$  and  $1M\Omega$  for both  $R_H$  and  $R_L$  to minimize power consumption under light loads. If  $V_{OUT}$  is 5V, a value of  $100k\Omega$  is chosen for  $R_H$ , then using the following equation,  $R_L$  can be calculated as  $13.7k\Omega$ :



#### Input Capacitor CIN

For the best performance, select a typical X5R or better grade ceramic capacitor with a 50V rating and at least  $2.2\mu$ F capacitance. The capacitor should be placed as close as possible to the device, while also minimizing the loop area formed by C<sub>IN</sub> and the IN/GND pins.

When selecting an input capacitor, ensure that its voltage rating is at least 20% greater than the maximum voltage of the input supply. X5R or X7R dielectric types are the most often selected due to their small size, low cost, surge current capability, and high RMS current rating over a wide temperature and voltage range.

In situations where the input rail is supplied through long wires, it is recommended to add some bulk capacitance like electrolytic, tantalum or polymer type capacitors to reduce the overshoot and ringing caused by the added parasitic inductance.



Consider the RMS current rating of the input capacitor, paralleling additional capacitors if required to meet the calculated RMS ripple current.

$$I_{CIN_{-RMS}} = I_{OUT} \times \sqrt{D \times (1 - D)}$$

The worst-case condition occurs at D = 0.5, then

$$I_{CIN\_RMS,MAX} = \frac{I_{OUT}}{2}$$

For simplicity, use an input capacitor with an RMS current rating greater than 50% of the maximum load current.

The input capacitor value determines the input voltage ripple of the converter. If there is a voltage ripple requirement in the system, choose an appropriate input capacitor that meets the specification.

Given the very low ESR and ESL of ceramic capacitors, the input voltage ripple can be estimated using the formula:

$$W_{CIN_{-}RIPPLE,CAP} = \frac{I_{OUT}}{f_{SW} \times C_{IN}} \times D \times (1 - D)$$

The worst-case condition occurs at D = 0.5, then

$$V_{CIN_{-RIPPLE,CAP,MAX}} = \frac{I_{OUT}}{4 \times f_{SW} \times C_{IN}}$$

The capacitance value is less important than the RMS current rating. A single  $2.2\mu$ F X5R capacitor is sufficient in most applications.

#### **Output Inductor L**

Consider the following when choosing this inductor:

 Choose the inductance to provide a ripple current that is approximately 40% of the maximum output current. The recommended inductance is calculated as:

$$L = \frac{V_{OUT}(1 - V_{OUT} / V_{IN,MAX})}{f_{sw} \times I_{OUT,MAX} \times 0.4}$$

Where  $f_{\text{SW}}$  is the switching frequency and  $I_{\text{OUT,MAX}}$  is the maximum load current.

The SY21061 has high tolerance for ripple current amplitude variation. As a result, the final choice of inductance can vary slightly from the calculated value with no significant performance impact.

2) The inductor's saturation current rating must be greater than the peak inductor current under full load:

$$I_{\text{SAT,MIN}} > I_{\text{OUT,MAX}} + \frac{V_{OUT} \left(1 - V_{OUT} / V_{\text{IN,MAX}}\right)}{2 \times f_{SW} \times L}$$

3) The DCR of the inductor and the core loss at the switching frequency must be low enough to achieve the desired efficiency requirement. Choose an inductor with DCR less than  $50m\Omega$  to achieve good overall efficiency.

#### Output Capacitor COUT

Select the output capacitor  $C_{OUT}$  to handle the output ripple requirements. Both steady state ripple and transient requirements must be taken into consideration when selecting the component. For the best performance, use an X5R or better grade ceramic capacitor with a 25V rating and capacitance greater than 22µF.

For applications where the design must meet stringent ripple requirements, the following considerations must be followed:

The output voltage ripple at the switching frequency is caused by the inductor current ripple ( $\Delta I_L$ ) on the output capacitor's ESR (ESR ripple), as well as the stored charge (capacitive ripple).

When calculating total ripple, consider both.

$$V_{RIPPLE.ESR} = \Delta I_L \times ESR$$

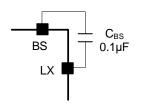
$$V_{RIPPLE,CAP} = \frac{\Delta I_L}{8 \times C_{OUT} \times f_{SW}}$$

The capacitive ripple might be higher because the effective capacitance for ceramic capacitors decreases with the voltage across the terminals. The voltage derating is usually included as a chart in the capacitor datasheet, and the ripple can be recalculated after taking the target output voltage into account.



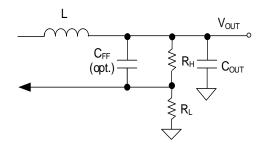
#### **External Bootstrap Capacitor**

This external bootstrap capacitor provides the gate driver voltage for internal power MOSFET. A  $0.1\mu$ F low-ESR ceramic capacitor connected between the BS pin and the LX pin is recommended.



#### Load Transient Consideration

The device integrates the compensation components to achieve good stability and fast transient responses. In some applications, adding a small ceramic capacitor in parallel with  $R_H$  may further speed up the load transient response. It is recommended for applications with large load transient step requirements.

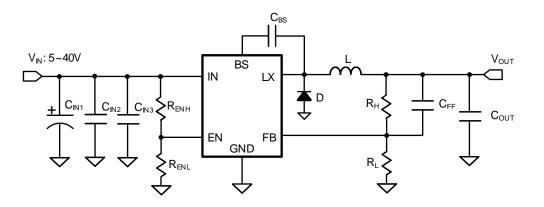


#### **Rectifier Diode**

To accommodate the device high switching speed, choose a Schottky diode with low forward voltage and fast switching speed. The diode's voltage rating must be higher than the Buck converter maximum input voltage, and the diode's average and peak current rating should be greater than the Buck converter output average current and peak current.



# Application Schematic (Vour=5V)



## **BOM List**

Designator	Description	Part Number	Manufacturer
C <sub>IN1</sub>	47µF/50V (electrolytic capacitor)		
CIN2	2.2µF/50V/1206	C3216X7R1H225K	TDK
CIN3, CBS	0.1µF/50V/0603	C1608X7R1H104K	TDK
Соит	22µF/16V/1206	C3216X5R1C226K	TDK
Cff	47pF/50V/0603	C1608C0G1H470J	TDK
D	3A/60V	SS36	
L	10µH/inductor, 3.2A	CDRH8D43NP-100NC	Sumida
Rн	100kΩ, 0603	RC0603FR-07100KL	
RL	13.7kΩ, 0603	RC0603FR-0713K7L	
Renh	10kΩ, 1%, 0603		
Renl	1MΩ, 1%, 0603		

### **Recommend Table for Typical Applications**

V <sub>OUT</sub> (V)	R <sub>H</sub> (kΩ)	R <sub>L</sub> (kΩ)	C <sub>FF</sub> (pF)	L/Part Number	C <sub>OUT</sub>
1.2	100	100	22	4.7µH/CDRH8D43NP-4R7NC	22µF/16V,1206,X5R
3.3	100	22.1	47	6.8µH/CDRH8D43NP-6R8NC	22µF/16V,1206,X5R
5	100	13.7	47	10µH/CDRH8D43NP-100NC	22µF/16V,1206,X5R



## Layout Design

Follow these PCB layout guidelines for optimal performance and thermal dissipation:

- **Input Capacitors:** Place the input capacitors close to the IN and GND pins, minimizing the loop formed by these connections. The input capacitor should be connected to the IN and GND using wide copper areas.
- **Output Capacitors:** Connect the C<sub>OUT</sub> negative terminal to the GND pin using wide copper traces instead of vias, in order to achieve better accuracy and stability of output voltage.
- Feedback Network: Place the feedback components (R<sub>H</sub>, R<sub>L</sub>, and C<sub>FF</sub>) as close to the FB pin as possible. Avoid routing the feedback line near LX, or other high-frequency signals as it is noise-sensitive. Use a Kelvin connection to connect with C<sub>OUT</sub> rather than the inductor output terminal.

- **LX Connection:** Keep the LX area small to prevent excessive EMI, while providing a wide copper area to minimize parasitic resistance and inductance.
- **EN Signal:** It is not recommended to connect EN signal directly to V<sub>IN</sub>. A resistor in a range of  $1k\Omega$  to  $1M\Omega$  should be used if the lines are pulled high to V<sub>IN</sub>.
- **GND Vias:** Place an adequate number of vias on the GND layer around the device for better thermal performance. The exposed GND pad should be connected to a copper area larger than its size. Place multiple GND vias on it for heat dissipation.
- **PCB Board:** To achieve the best thermal and noise performance, maximize the PCB copper area connecting to the GND pin. A ground plane is highly recommended if board space allows. Connect the ground pad to a large copper area to enhance thermal performance.

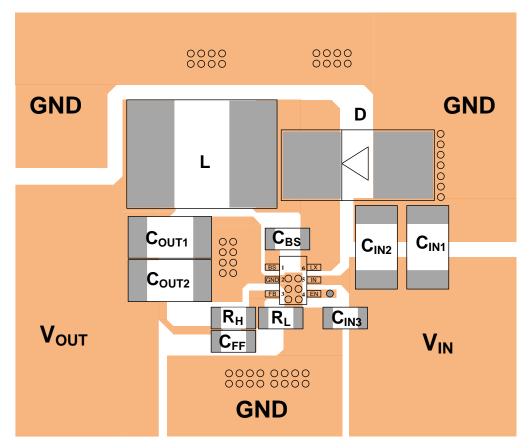
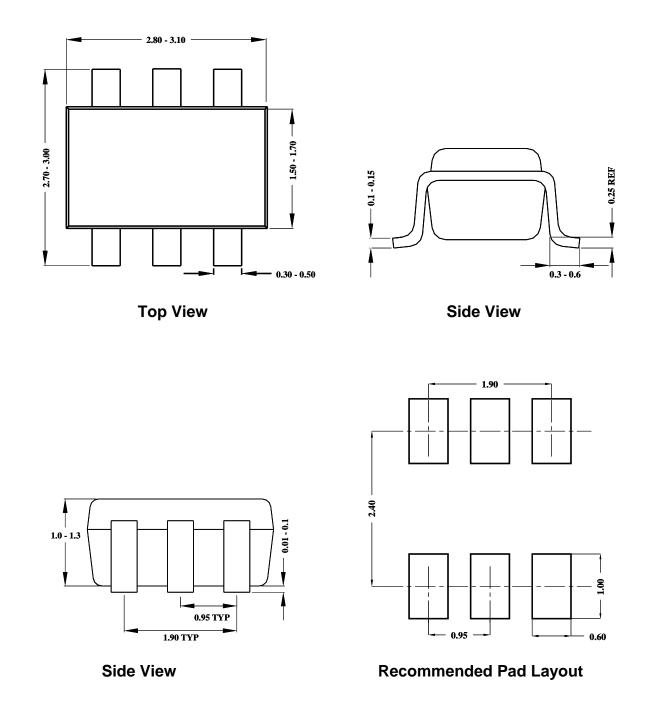


Figure 4. Suggested PCB Layout





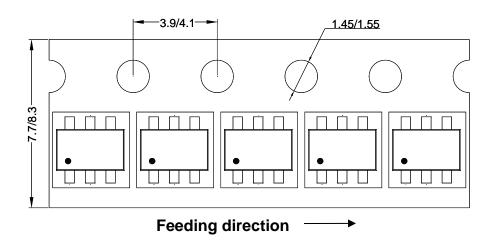


Notes: All dimension in millimeter and exclude mold flash & metal burr.

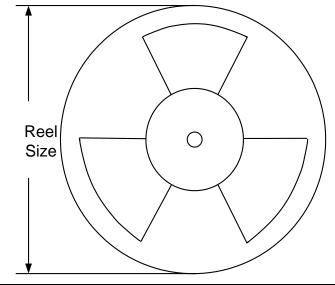


# **Taping & Reel Specification**

### **SOT23-6 Taping Orientation**



### Carrier Tape & Reel Specification for Packages



Package	Tape width	Pocket	Reel size	Trailer	Leader length	Qty per
types	(mm)	pitch(mm)	(Inch)	length(mm)	(mm)	reel
SOT23-6	8	4	7"	280	160	3000

### Others: NA



### **Revision History**

The revision history provided is for informational purposes only and is believed to be accurate; however, it is not warrantied. Please make sure that you have the latest revision.

Date	Revision	Change
Nov. 16, 2014	Revision 0.9	Initial Release
Aug. 30, 2023	Revision 1.0	Production Release



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