

High Efficiency, 8.0A 40V Input Synchronous Step Down Regulator

General Description

The SY8308 develops a high efficiency synchronous step-down DC/DC regulator capable of delivering 8A continuous current. The device integrates main switch and synchronous switch with very low $R_{DS(ON)}$ to minimize the conduction loss.

The SY8308 operates over a wide input voltage range from 4V to 40V. The device adopts the instant PWM architecture to achieve fast transient responses for high step down applications and high efficiency at light loads.

Ordering Information

SY8308 □(□□)□
 □ Temperature Code
 □ Package Code
 □ Optional Spec Code

Ordering Number	Package type	Note
SY8308RBC	QFN3.5×3.5-20	--

Features

- Low $R_{DS(ON)}$ for Internal Switches (Top/Bottom): 25mΩ/12mΩ
- 4~40V Input Voltage Range
- 8.0A Output Current Capability
- Selectable 350 kHz/500kHz Switching Frequency
- PFM/PWM Selectable Light Load Operation Mode
- Instant PWM Architecture to Achieve Fast Transient Responses.
- Programmable Soft-start Limits the Inrush Current
- Programmable Valley Current Limit Threshold
- Hic-cup Mode Output Short Circuit Protection
- Power Good Indicator
- 0.6V±1% Reference Voltage
- Compact Package: QFN3.5×3.5-20

Applications

- LCD-TV
- SetTop Box
- Notebook
- Storage
- High Power AP Router
- Networking

Typical Applications

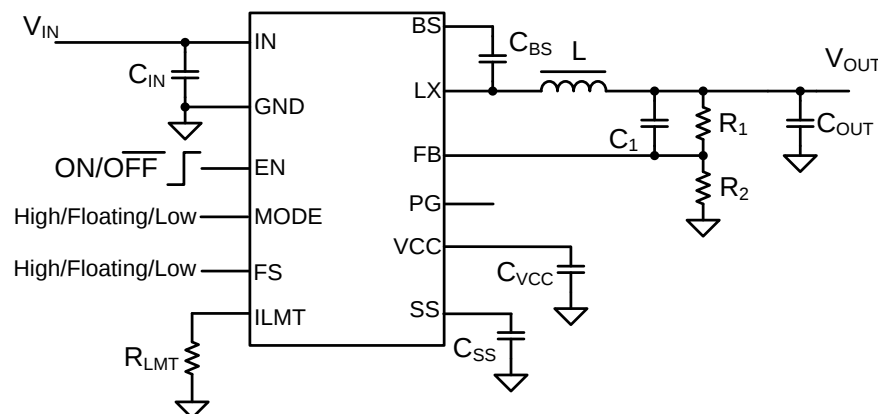
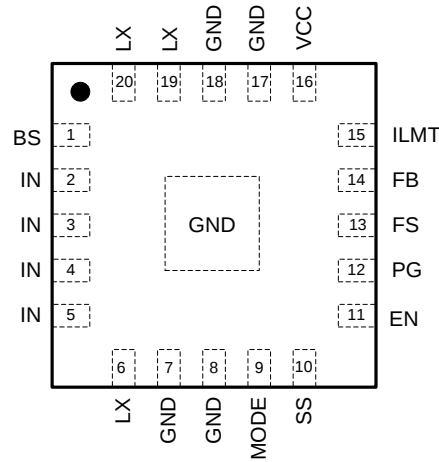


Figure1. Schematic Diagram

Pinout (top view)



(QFN3.5x3.5-20)

Top Mark: BDYxyz, (Device code: BDY, x=*year code*, y=*week code*, z= *lot number code*)

Pin Name	Pin Number	Pin Description
BS	1	Boot-strap pin. Supply high side gate driver. Connect a 0.1μF ceramic capacitor between the BS and the LX pin.
IN	2,3,4,5	Input pin. Decouple this pin to the GND pin with at least a 10μF ceramic capacitor.
LX	6,19,20	Inductor pin. Connect this pin to the switching node of the inductor.
GND	7,8,17,18, Exposed pad	Ground pin.
MODE	9	Operating mode selection under light load. Pull this pin low for PFM operating; pull this pin high or floating for PWM operation.
SS	10	Soft-start programming pin. Connect a capacitor from this pin to ground to program the soft-start time. $t_{ss}(ms)=C_{ss}(nF) \times 0.6V/6\mu A$. Leave this pin open for default 1ms soft-start.
EN	11	Enable control. Pull high to turn on. Do not leave it floating.
PG	12	Power good Indicator. Open-drain output when the output voltage is within 85% to 122% of regulation point.
FS	13	Switching frequency selection. Pull this pin low for 350kHz; pull this pin high or floating for 500kHz.
FB	14	Output feedback pin. Connect this pin to the center point of the output resistor divider (as shown in Figure 1) to program the output voltage: $V_{OUT}=0.6 \times (1+R_1/R_2)$.
ILMT	15	Valley current limit programming. $I_{LMT_VALLEY}(A)=3600/R_{LMT}(k\Omega)$. Leave this pin open for default 6A valley current limit threshold.
VCC	16	Internal 3.3V output. Decouple this pin to ground with at least a 4.7μF capacitor.

Block Diagram

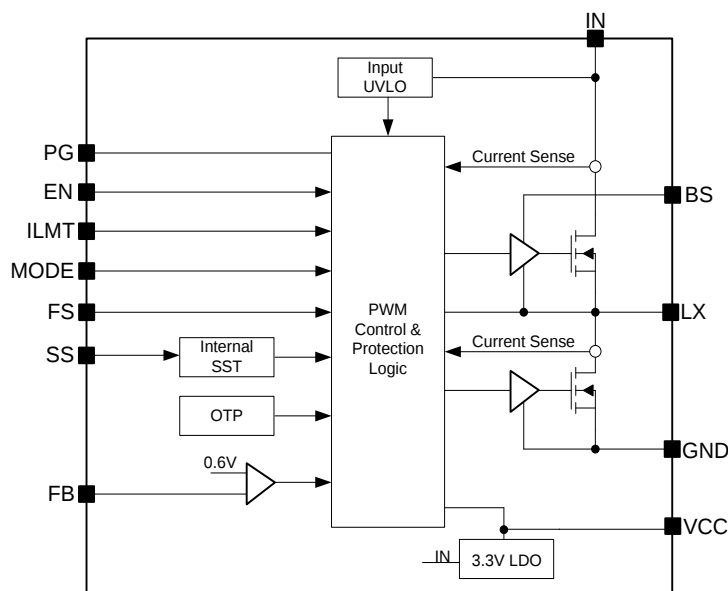


Figure2. Block Diagram

Absolute Maximum Ratings (Note 1)

Supply Input Voltage	-0.3V to 40V
BS-LX, VCC, FB Voltage	-0.3V to 4V
LIMIT, FS, PG, EN, MODE, SS, LX Voltage	-0.3V to VIN + 0.3V
Power Dissipation, PD @ TA = 25°C, QFN3.5×3.5-20	3.6W
Package Thermal Resistance (Note 2)	
ΘJA	28°C/W
ΘJC	4°C/W
Junction Temperature Range	-40°C to 150°C
Lead Temperature (Soldering, 10 sec.)	260°C
Storage Temperature Range	-65°C to 150°C
Dynamic LX voltage in 10ns duration	IN+3V to GND-5V

Recommended Operating Conditions (Note 3)

Supply Input Voltage	4V to 40V
Junction Temperature Range	-40°C to 125°C

Electrical Characteristics

($V_{IN} = 12V$, $T_A = 25^{\circ}C$, $I_{OUT} = 1A$, unless otherwise specified)

Parameter	Symbol	Test Conditions	Min	Typ	Max	Unit
Input Voltage Range	V_{IN}		4		40	V
Input UVLO Threshold	V_{UVLO}				3.9	V
Input UVLO Hysteresis	V_{HYS}			0.3		V
Quiescent Current	I_Q	$I_{OUT}=0$, $V_{FB}=V_{REF}\times 105\%$		60		μA
Shutdown Current	I_{SHDN}	$EN=0$			4	μA
Feedback Reference Voltage	V_{REF}		0.594	0.6	0.606	V
FB Input Current	I_{FB}	$V_{FB}=3.3V$	-50		50	nA
Top FET RON	$R_{DS(ON)1}$			25		m Ω
Bottom FET RON	$R_{DS(ON)2}$			12		m Ω
Bottom FET Valley Current Limit Program Range	$I_{LMT,RNG}$	$R_{LMT}=300k\Omega\sim 600k\Omega$	6		12	A
Bottom FET Valley Current Limit Setting Accuracy	I_{LMT}	$R_{LMT}=300k\Omega$	9.6	12	14.4	A
Bottom FET Reverse Current Limit	$I_{LMT,RVS}$	MODE=High	3.5			A
EN Input Voltage High	$V_{EN,H}$		1.5			V
EN Input Voltage Low	$V_{EN,L}$				0.4	V
EN Leakage Current	I_{EN}				1	μA
MODE Input Voltage High	$V_{MODE,H}$		$V_{CC}-0.8$			V
MODE Input Voltage Low	$V_{MODE,L}$				0.4	V
MODE Leakage Current	I_{MODE}				1	μA
FS Input Voltage High	$V_{FS,H}$		$V_{CC}-0.8$			V
FS Input Voltage Low	$V_{FS,L}$				0.4	V
FS Leakage Current	I_{FS}				1	μA
Power Good Threshold	$V_{PG,TH}$	V_{FB} falling, PG from high to low	81	85	89	$\%V_{REF}$
		V_{FB} rising, PG from low to high	85	90	95	$\%V_{REF}$
		V_{FB} falling, PG from low to high	104	110	116	$\%V_{REF}$
		V_{FB} rising, PG from high to low	116	122	128	$\%V_{REF}$
Power Good Delay	$t_{PG,DLY}$	Low to high		200		μs
		High to low		10		μs
Power Good Low Voltage	V_{PG_LOW}	Sink 5mA to PG pin, $FB=0.6V$			0.4	V
Soft-start Charging Current	I_{SS}			6		μA
Internal Soft-start Time	t_{SS}	SS floating		1		ms
Output Over Voltage Threshold	V_{OVP}	V_{FB} rising	116	122	128	$\%V_{REF}$
Output Over Voltage Hysteresis	$V_{OVP,HYS}$			10		$\%V_{REF}$
Output OVP Delay	$t_{OVP,DLY}$			15		μs
Output Under Voltage Protection Threshold	$V_{OUT,UVF}$	V_{FB} falling	45	50	55	$\%V_{REF}$
Output UVP Delay	$t_{UVP,DLY}$			200		μs
UVF Hic-cup ON Time	$t_{UVP,ON}$	SS floating		3		ms
UVF Hic-cup OFF Time	$t_{UVP,OFF}$	SS floating		21		ms
Switching Frequency	f_{SW}	FS=Floating, CCM	400	500	600	kHz
VCC Output Voltage	V_{VCC}		3.15	3.3	3.45	V

Parameter	Symbol	Test Conditions	Min	Typ	Max	Unit
Min ON Time	$t_{ON,MIN}$			80		ns
Min OFF Time	$t_{OFF,MIN}$			160		ns
Thermal Shutdown Temperature	T_{SD}			150		°C
Thermal Shutdown Hysteresis	T_{HYS}			15		°C

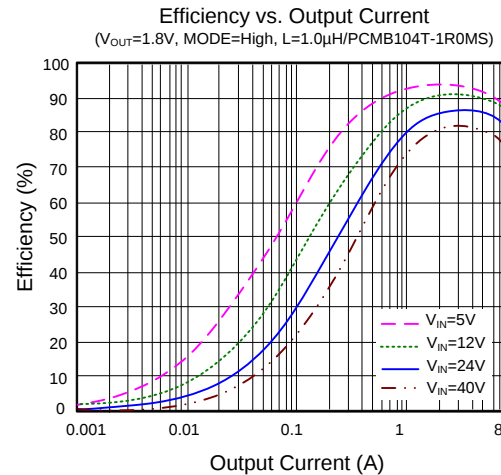
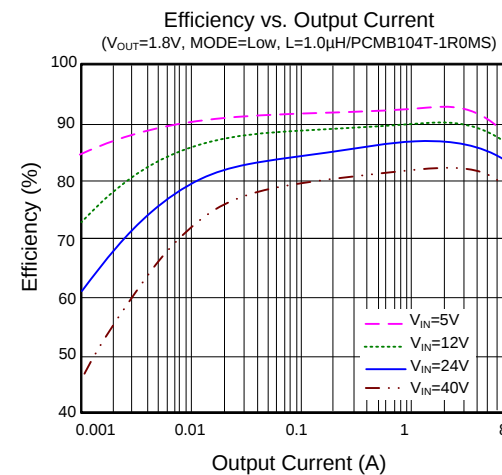
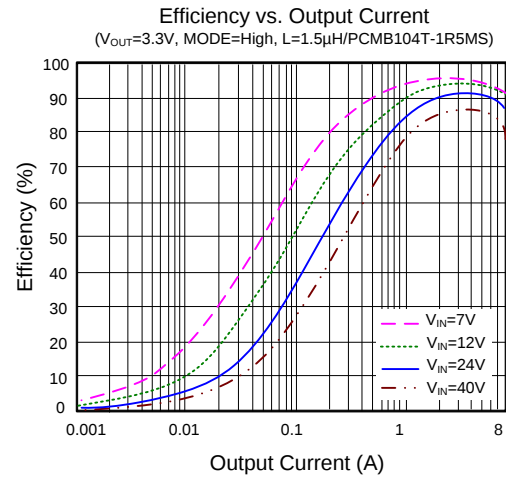
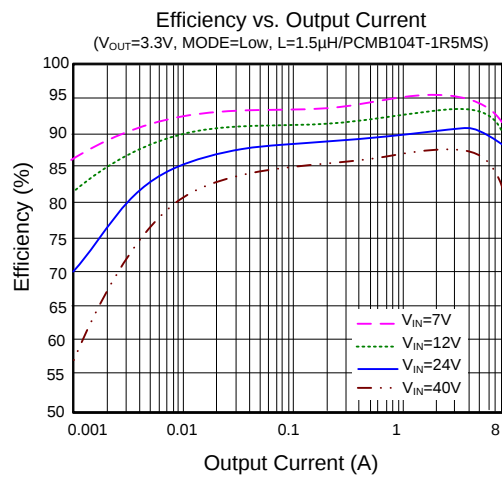
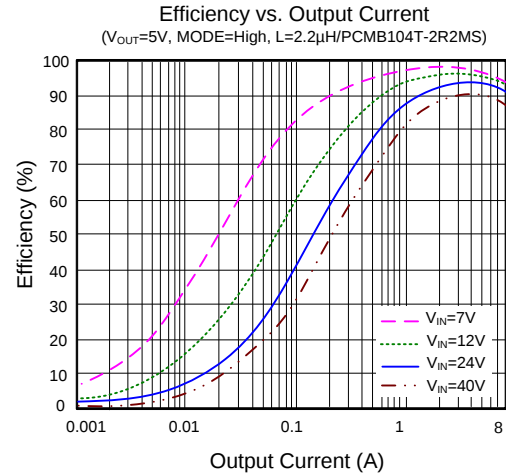
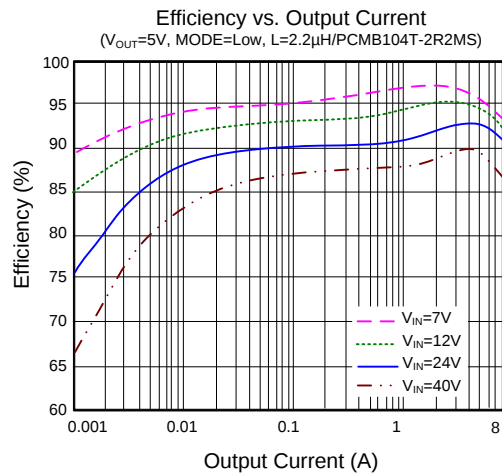
Note 1: Stresses beyond the “Absolute Maximum Ratings” may cause permanent damage to the device. These are stress ratings only. Functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

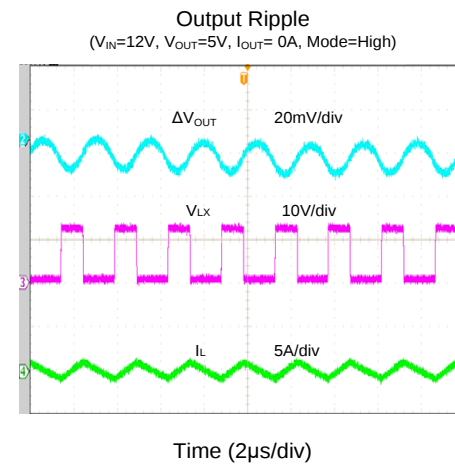
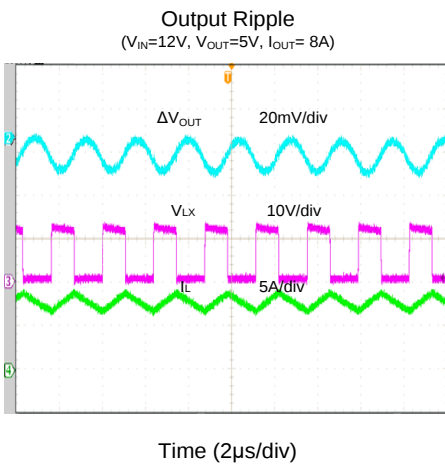
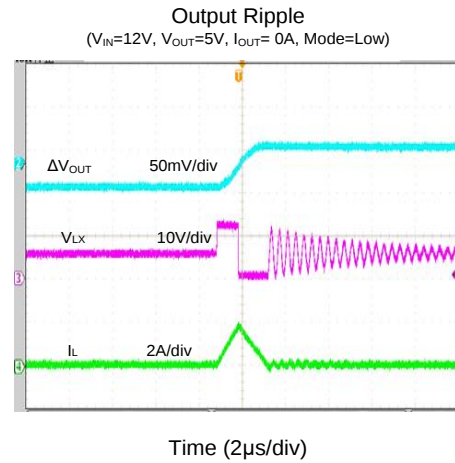
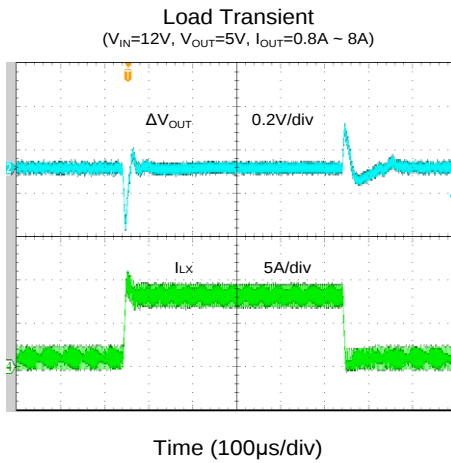
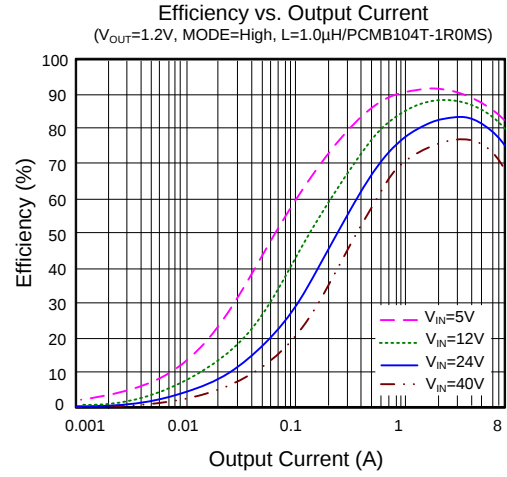
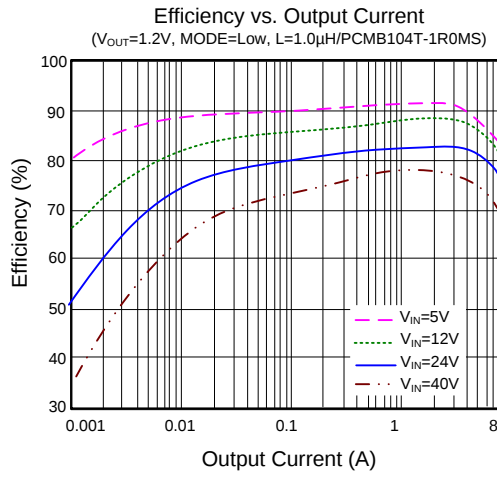
Note 2: Package thermal resistance is measured in the natural convection at $T_A = 25^{\circ}\text{C}$ on a four-layer Silergy Evaluation Board.

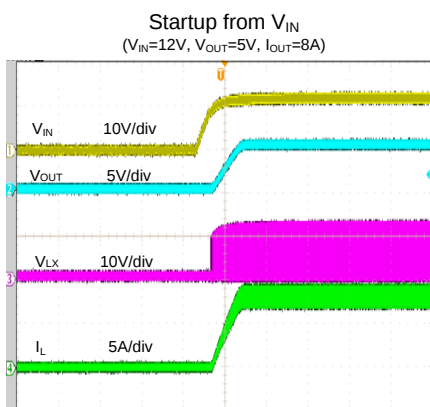
Note 3: The device is not guaranteed to function outside its operating conditions.

Typical Performance Characteristics

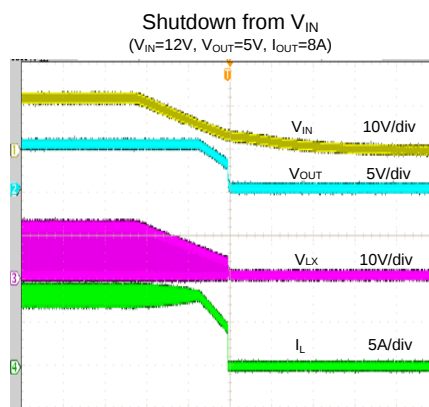
($f_{sw}=500kHz$, $T_A = 25^\circ C$)



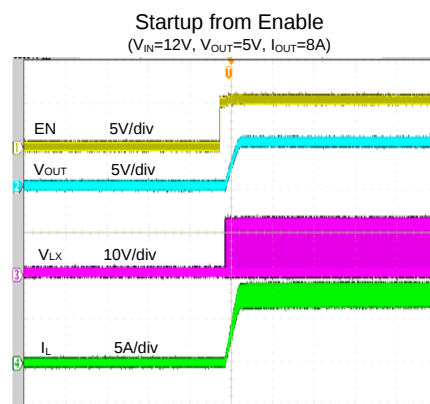




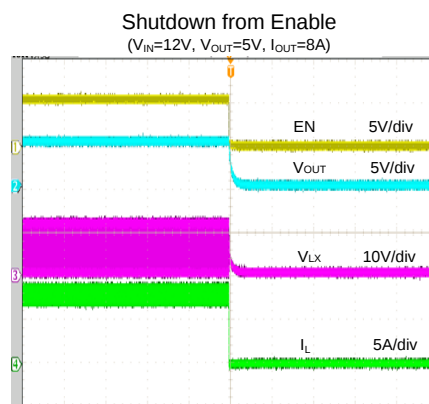
Time (2ms/div)



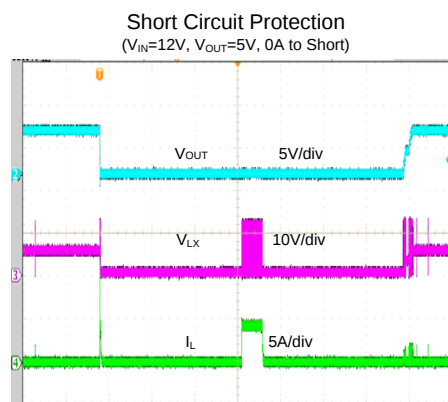
Time (4ms/div)



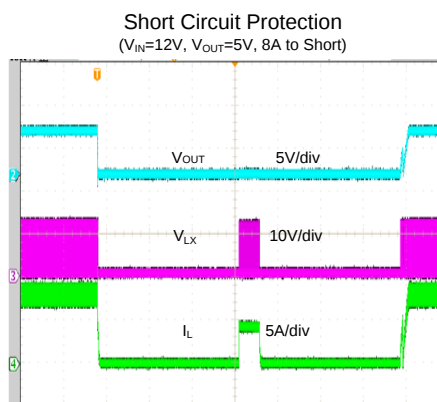
Time (4ms/div)



Time (800 μ s/div)



Time (10ms/div)



Time (10ms/div)

Operation

The SY8308 develops a high efficiency synchronous step-down DC/DC regulator capable of delivering 8A current. The device integrates a main switch and a synchronous switch with very low $R_{DS(ON)}$ to minimize the conduction loss.

The SY8308 operates over a wide input voltage range from 4V to 40V. The DC/DC regulator adopts the instant PWM architecture to achieve fast transient responses for high step down applications and high efficiency at light load. The device provides various protection features for reliable operation.

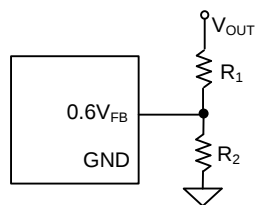
Applications Information

Because of the high integration in the SY8308, the application circuit based on this regulator is rather simple. Only the input capacitor C_{IN} , the output capacitor C_{OUT} , the output inductor L and the feedback resistors (R_1 and R_2) need to be selected for the targeted applications specifications.

Feedback Resistor Dividers R_1 and R_2

Choose R_1 and R_2 to program the proper output voltage. To minimize the power consumption under light load, it is desirable to choose large resistance values for both R_1 and R_2 . A value of between $10k\Omega$ and $1M\Omega$ is highly recommended for both resistors. If V_{OUT} is 1.2V, $R_1=100k\Omega$ is chosen, then using the following equation, R_2 can be calculated to be $100k\Omega$:

$$R_2 = \frac{0.6V}{V_{OUT} - 0.6V} \times R_1$$



Input Capacitor C_{IN}

The ripple current through input capacitor is calculated as:

$$I_{CIN_RMS} = I_{OUT} \times \sqrt{D \times (1-D)}$$

To minimize the potential noise problem, place a typical X5R or better grade ceramic capacitor really close to the IN and GND pins. Care should be taken to

minimize the loop area formed by C_{IN} , and IN/GND pins. In this case, a $10\mu F$ low ESR ceramic capacitor is recommended.

Output Capacitor C_{OUT}

The output capacitor is selected to handle the output ripple noise requirements. Both steady state ripple and transient requirements must be taken into consideration when selecting this capacitor. For most applications, an X5R or better grade ceramic capacitor larger than $66\mu F$ capacitance can work well. The capacitance derating with DC voltage must be considered.

Output Inductor L

There are several considerations in choosing this inductor.

- 1) Choose the inductance to provide the desired ripple current. It is suggested to choose the ripple current to be about 40% of the maximum output current. The inductance is calculated as:

$$L = \frac{V_{OUT}(1 - V_{OUT}/V_{IN,MAX})}{f_{SW} \times I_{OUT,MAX} \times 40\%}$$

where f_{sw} is the switching frequency and $I_{OUT,MAX}$ is the maximum load current.

The SY8308 is quite tolerant of different ripple current amplitude. Consequently, the final choice of inductance can be slightly off the calculation value without significantly impacting the performance.

- 2) The saturation current rating of the inductor must be selected to be greater than the peak inductor current under full load condition.

$$I_{SAT, MIN} > I_{OUT, MAX} + \frac{V_{OUT}(1 - V_{OUT}/V_{IN,MAX})}{2 \times f_{SW} \times L}$$

- 3) The DCR of the inductor and the core loss at the switching frequency must be low enough to achieve the desired efficiency requirement. It is desirable to choose an inductor with $DCR < 10m\Omega$ to achieve a good overall efficiency.

Enable Operation

Pulling the EN pin low will shut down the device. During shutdown mode, the SY8308 shutdown current drops to lower than $4\mu A$. Driving the EN pin high will turn on the IC again.

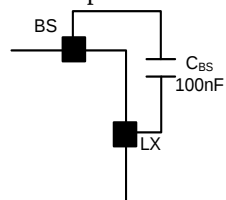
Soft-start

The SY8308 provides programmable soft-start time feature. The minimum soft-start time is 1ms typically when SS pin is floating. Connect a capacitor across the SS pin and GND to program the soft-start time.

$$t_{ss}(ms) = C_{ss}(nF) \times \frac{0.6(V)}{6(\mu A)}$$

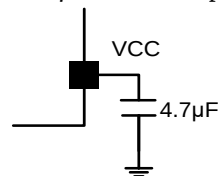
External Bootstrap Capacitor

This capacitor provides the gate driver voltage for internal high side MOSEFET. A 100nF low ESR ceramic capacitor connected between the BS pin and the LX pin is recommended.



VCC LDO

The 3.3V VCC LDO provides the power supply for internal control circuit. Bypass this pin to ground with a 4.7μF ceramic capacitor.



Power Good Indication

PG is an open-drain output pin. This pin will pull to ground if output voltage is lower than 85% or higher than 122% of the regulation voltage. Otherwise this pin will go to a high impedance state.

Switching Frequency Select

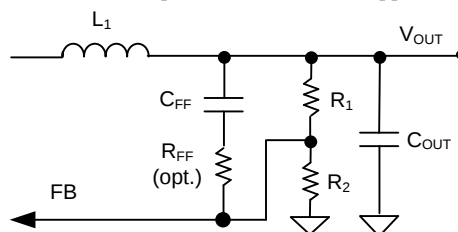
350kHz or 500kHz switching frequency can be selected by the FS pin. Pull this pin low for 350kHz; pull this pin high or floating for 500kHz.

Light Load Operation Mode Selection

PFM or PWM light load operation is selected by the MODE pin. Pull the MODE pin low for PFM operation, and pull this pin high or floating for PWM operation.

Load Transient Considerations

The SY8308 adopts the instant PWM architecture to achieve good stability and fast transient responses. In applications with high step load current, adding an RC network R_{FF} and C_{FF} parallel with R_1 may further speed up the load transient responses. $R_{FF} = 1k\Omega$ and $C_{FF} = 470pF$ have shown to perform well in most applications.



Over-current Protection (OCP)

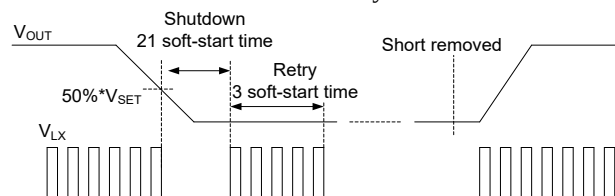
SY8308 incorporates a cycle-by-cycle valley current limit. Inductor current is measured in the synchronous rectifier when it is on and as the inductor current ramps down. If the current exceeds the current limit, HS FET turn-on is inhibited until the current returns to safe levels.

The valley current limit can be programmed with a resistor R_{LMT} connecting from ILMT pin to ground:

$$I_{LMT_VALLEY}(A) = \frac{3600}{R_{LMT}(k\Omega)}$$

Short-circuit protection (SCP)

If $V_{OUT} < 50\%$ of the set-point continuously for approximately 200μs, the short-circuit protection mode will be initiated, and the device will shut down for 21 soft-start time. The device will then restart and keep working for 3 soft-start time. If the short circuit condition remains, another 'hiccup' cycle of shutdown and restart will continue indefinitely.



Over-temperature Protection (OTP)

The device includes over-temperature protection (OTP) circuitry to prevent overheating due to excessive power dissipation. This will shut down switching operation when the junction temperature exceeds 150°C. Once the junction temperature cools down by approximately 15°C the IC will resume normal operation after a complete soft-start cycle. For continuous operation, provide adequate cooling so that the junction temperature does not exceed the OTP threshold.

Layout Design

The layout design of SY8308 is relatively simple. For the best efficiency and minimum noise problem, the following components should be close to the IC: C_{IN} , C_{VCC} , L , R_1 and R_2 .

- 1) It is desirable to maximize the PCB copper area connecting to the GND pin to achieve the best thermal and noise performance. If the board space allows, a ground plane is highly desirable.

- 2) C_{IN} must be close to the IN and GND pins. The loop area formed by C_{IN} and GND must be minimized.
- 3) The PCB copper area associated with the LX pin must be minimized to avoid the potential noise problem.
- 4) The components R_1 and R_2 and the trace connecting to the FB pin must NOT be adjacent to the LX net on the PCB layout to avoid the noise problem.
- 5) If the system chip interfacing with the EN pin has a high impedance state at shutdown mode and the IN pin is connected directly to a power source such as a Li-Ion battery. A 1M Ω pull down resistor should be placed between the EN and GND pins to prevent the noise from falsely turning on the regulator at shutdown mode.

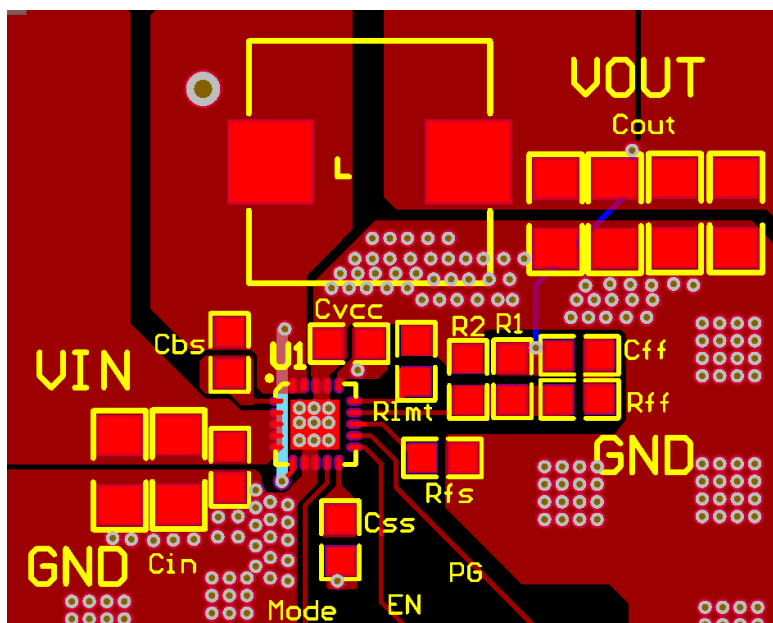
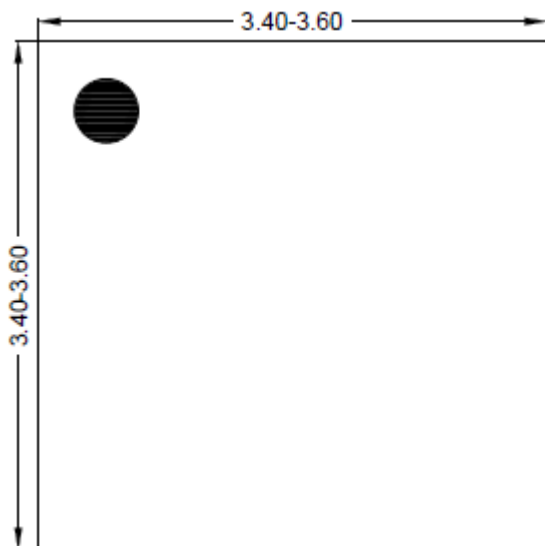
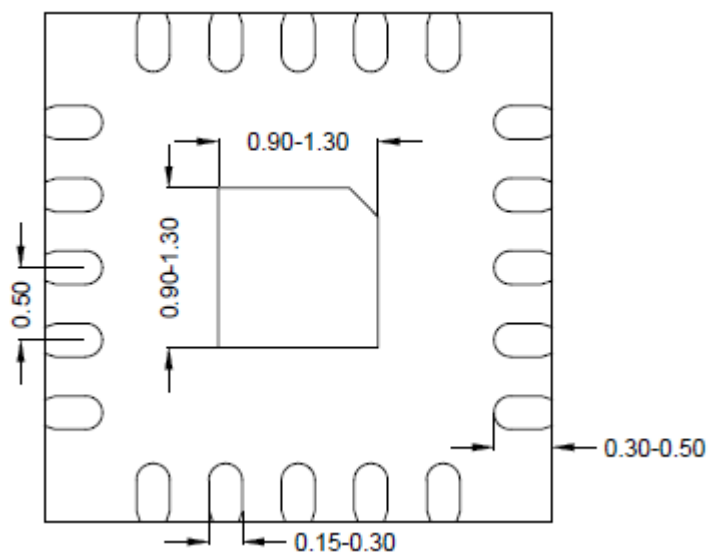


Figure3. PCB Layout Suggestion

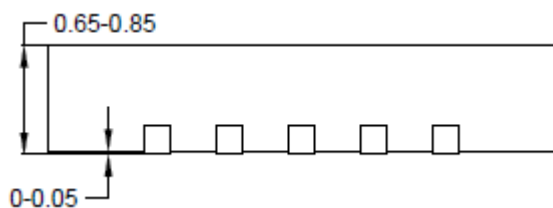
QFN3.5×3.5-20 Package Outline



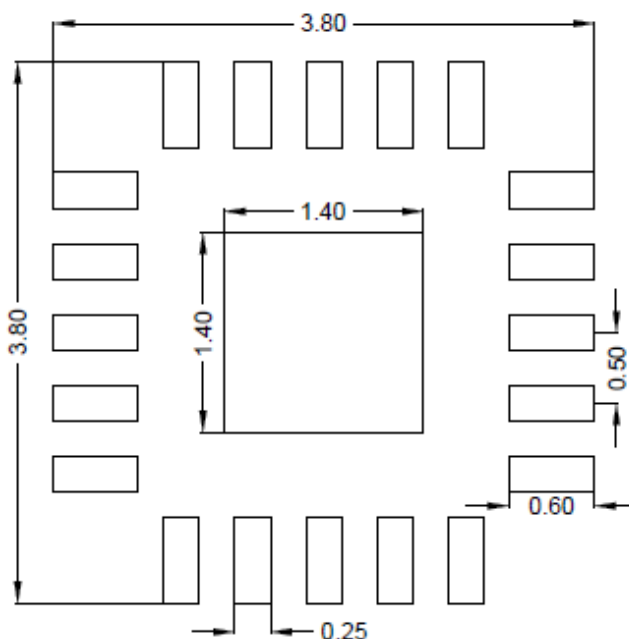
Top view



Bottom view



Side view

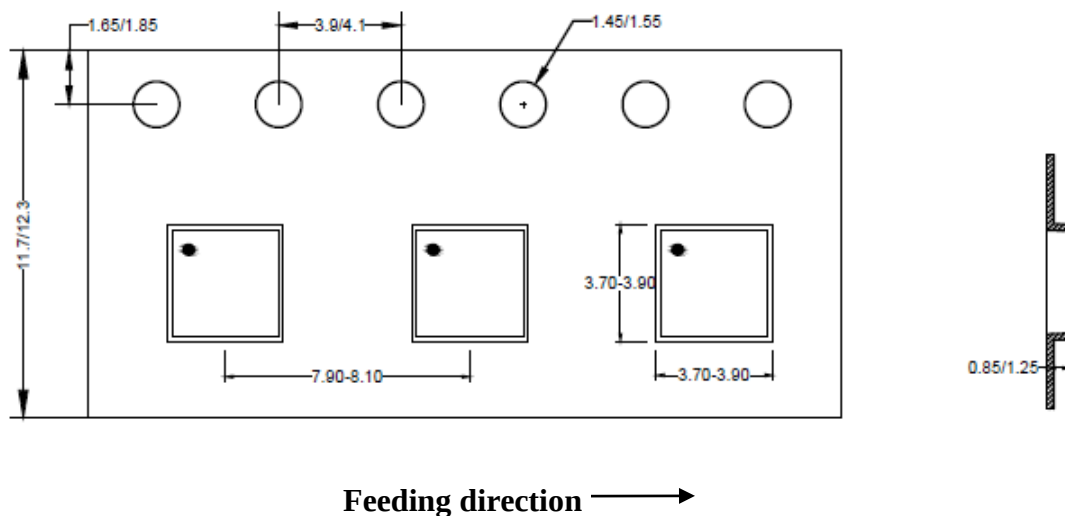


**Recommended PCB layout
(Reference only)**

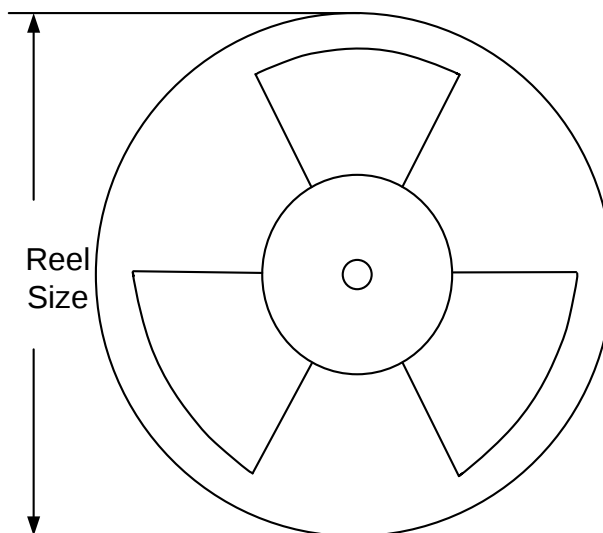
Notes: All dimension in millimeter and exclude mold flash & metal burr.

Taping & Reel Specification

1. QFN3.5×3.5-20 taping orientation



2. Carrier Tape & Reel specification for packages



Package types	Tape width (mm)	Pocket pitch(mm)	Reel size (Inch)	Trailer length(mm)	Leader length (mm)	Qty per reel
QFN3.5×3.5	12	8	13"	400	400	3000

3. Others: NA



Revision History

The revision history provided is for informational purpose only and is believed to be accurate, however, not warranted. Please make sure that you have the latest revision.

Date	Revision	Change
Nov.25, 2020	Revision 0.9	Initial Release

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